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TRIP-TRAJECTORY INTEGRATION PROGRAM

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TRIP-TRAJECTORY INTEGRATION PROGRAM

Bernard Kaufman

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ABSTRACT

This document describes a numerical integration program (TRIP) based on Encke's method of integrating only the perturbations in the cartesian coordinates. The mathematical model can include Venus, Earth, Mars, Jupiter, the Moon and the Sun as either central or disturbing bodies. In addition, full oblateness potentials are included for the Earth and Moon and J_2 only for Mars. Modification to expand the oblateness models for the other planets is simple. Solar radiation pressure may also be included as an option in the input. The program uses the latest exported JPL double precision planetary ephemerides (DE 19)

TRIP has the option of calculating shadow times using penumbra and umbra; and printout may be obtained at specified times or, in the case of a planetary orbiter, at apoapsis or periapsis. Input data is very simple and there is a variety of coordinate systems for printout.

TRIP is available from the Goddard Program Library under number D00140. It is a 360/95 program and has proven over the years to be accurate and very fast.

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TRIP-TRAJECTORY INTEGRATION PROGRAM

INTRODUCTION

TRIP was developed in 1968 primarily to provide an accurate and fast trajectory program to replace the n-body numerical integration programs then in use for mission analysis at Goddard. These were primarily large and very slow programs such as the old JPL Space Program. A second and equally important objective was to make the input format simple enough to be used without extensive study of a manual.

TRIP was developed along modular lines so that it could be easily modified. It uses a fourth-order predictor-corrector numerical integration subroutine (described later) which because of the modularity may be easily replaced by any integration package. Many options have been added to TRIP since it was first developed; however, since Encke's method is used which requires rectification of the reference orbit, it was not considered advantageous to incorporate atmospheric drag.

Throughout the development of TRIP, its speed and simplicity have been maintained, making it a very useful as well as accurate, tool. It was most recently used for the launch window analysis for Imp-I.

TRIP is currently running on the IBM 360/95 and is available in the Goddard program library (number D00140).

DESCRIPTION OF SUBROUTINES

The functions of the subroutines used in TRIP are described briefly below. Many of them came from the Quick Look Mission Analysis Program developed by Philco-Ford (reference 1). A complete listing of TRIP appears in Appendix A.

- MAIN - The driver for TRIP. Its primary function is to set up certain keys from the input data.
- ADOT - (Reference 1) Obtains the angle between two vectors.
- ARES - (Reference 2) Calculates the matrix necessary to transform coordinates from Earth mean equinox and equator of date to Mars mean equinox and equator of date.

- ARKTNS - (Reference 1) Obtains the arctangent of y/x .
- CROSS - (Reference 1) Finds the cross product of two 3-dimensional vectors
- DERIV - Calculates the disturbing accelerations due to the presence of other bodies and, when required, calls other subroutines to calculate accelerations due to oblateness and solar radiation pressure. Performs rectification test.
- DOT - (Reference 1) Finds the dot product of two vectors.
- FNOL II - (Reference 3) Used for the numerical integration of a system of ordinary differential equations. A fourth-order Adams-Moulton predictor-corrector with a Runge-Kutta starter, FNOL II has the option of automatically varying the step size.
- FNORM - (Reference 1) Finds the magnitude of a 3-dimensional vector.
- GETACC - (Reference 4) Evaluates the disturbing acceleration due to oblateness of the Moon or Earth.
- GETTAP - (Reference 5) Used to position the ephemeris data set and read the correct data record.
- GHA - (Reference 1) Calculates the Greenwich hour angle.
- GOTOR - (Reference 1) Solves Kepler's equation for incremental eccentric anomaly on a conic section given the incremental mean anomaly (time).
- HARMON - Computes acceleration due to oblateness of Mars and is the driver for GETACC
- INTR1 - (Reference 5) Sets up the call to READE to find position and velocity of the other bodies with respect to the central body.
- ITER - Calculates times of entrances and exits from penumbra and umbra.
- KONSTK - Defines all constants needed by TRIP.
- M1 - (Reference 1) Multiplies a 3-dimensional vector by a 3×3 matrix.

- MNA - (Reference 1) Provides the matrix to transform moon-centered coordinates in Earth's true equator and equinox to Moon-centered coordinates in the moon's true equator.
- MULT - (Reference 1) Forms the product of two 3×3 matrices.
- NUTAIT - (Reference 1) Calculates the matrix to relate coordinates in Earth's mean equator and equinox to the true equator and equinox.
- ORB - (Reference 1) Transforms cartesian state vector to keplerian elements.
- ORB2X - (Reference 1) Transforms keplerian elements to cartesian state vector.
- OUT - Prints out various types of output as determined by keys set from input.
- OUTX - (Reference 1) Prints out cartesian and spherical coordinates. Called from subroutine OUT.
- OVERLAY - (Reference 1) Reads input data.
- READE - (Reference 5) Reads, interpolates and translates ephemeris data from the JPL double-precision ephemeris system (DE-19).
- ROTEQ - (Reference 1) Provides the matrix to transform from mean equator and equinox of 1950.0 to mean equator and equinox of date.
- RVOUT - (Reference 1) Calculates spherical coordinates of position and velocity.
- SHADOW - Driver for subroutine ITER. Sets up keys to be used in calculating shadow times.
- SHIFTP - (Reference 1) Provides the cartesian state vector of a probe relative to all the bodies in the ephemeris.
- SOLAR - Calculates the perturbing acceleration due to solar radiation pressure.
- SPER - (Reference 1) Converts cartesian position to spherical coordinates.

- STEPPD - (Reference 1) Obtains the state vector of a probe which is separated from an initial state by a time or angle increment, assuming only two-body motion.
- TCONIC - (Reference 1) Calculates time from periapsis corresponding to a given true anomaly on a conic section.
- TERM - Contains termination logic for the numerical integrator. Determines when the proper conditions for termination have occurred.
- TFRAC - (Reference 1) Provides the integral and fractional parts of the sum of two numbers.
- TIMEC - (Reference 1) Computes whole and fractional days from January 1, 1950 at 0^{hr}.
- TRAJ - The driver for FNOL II.

INPUT

All constants and variables needed for the program are contained in subroutine KONSTK and built-in values are supplied there for everything except the state vector and the epoch times. The state vector, option keys and epoch times are input through subroutine OVRLAY, which also provides for overlaying any of the built-in constants or variables. A complete description of the input necessary to run TRIP is given below.

The input format is 4 (I3, D12.8). The first 3 digits are fixed-point input (I3) and represent the C-array location of the variable in subroutine KONSTK. The C-array location is followed by the value desired.

<u>C-array</u>	<u>Name (if any)</u>	<u>Variable</u>
750		X (km) or a (km)
751		Y (km) or e
752		Z (km) or θ (true anomaly-deg.)
753		\dot{X} (km/sec) or Ω (deg)
754		\dot{Y} (km/sec) or i (deg)
755		\dot{Z} (km/sec) or ω (deg)
756		Epoch time (year, month, day in form of yymm.dd)
757		Epoch time (hour, minutes, seconds in form of hhmm.sec)

758	Type	Reference coordinate system of input 1. Earth mean equator and equinox of 1950, 0 ^h , Jan. 1, 2. True ecliptic and equinox of date, 3. Selenographic-true moon equator — <u>rotating</u> , 4. Mars mean equator of date, 5. True Earth equator and equinox of date.
759		Stop time (year, month, day as above)
760		Stop time (hours, minutes, seconds as above)
761	TINC (days)	TINC = total days from start to stop time if only <u>1st and last point</u> , or printout at <u>periapsis</u> or <u>apoapsis</u> is wanted, or printout at <u>approximate steps</u> of Δt is wanted (nearest time step to Δt). TINC = Δt if printout at <u>exact</u> intervals of Δt is wanted. Built-in value is 180. (days)
762	TOTAL (≥ 1) =	<div style="display: flex; align-items: center;"> <div style="font-size: 4em; margin-right: 10px;">{</div> <div> 1. If printout is wanted at the <u>1st and last points</u> only, or if printout at <u>periapsis</u> or <u>apoapsis</u> is wanted, or if printout is wanted at <u>approximate steps</u> of Δt. <div style="display: flex; align-items: center;"> <div style="text-align: center; margin-right: 20px;"> $\frac{\text{total days}}{\Delta t}$ </div> <div> If printout is wanted at <u>exact</u> steps of Δt. </div> </div> </div> </div> Built-in value is 1. For printout at exact steps, an additional print occurs if $\text{TOTAL} * \Delta t \neq \text{stop time}$.
763	XM (reference 3)	<div style="display: flex; align-items: center;"> <div style="font-size: 4em; margin-right: 10px;">{</div> <div> 100 000. If printout at <u>1st and last points</u> is wanted, or if printout is wanted at <u>periapsis</u>, <u>apoapsis</u> or <u>exact intervals</u> of Δt. 0. If printout is wanted at <u>approximate steps</u> of Δt </div> </div> Built-in value is 0.

764 Y(8) (reference 3) = $\begin{cases} 0. & \text{If printout is wanted at first and last points only; or if printout is wanted at periapsis, apoapsis or exact steps of } \Delta t. \\ \Delta t \text{ (seconds)} & \text{If printout is wanted at approximate steps of } \Delta t. \end{cases}$

Built-in value is 86400. (seconds)

765 SHADOW = $\begin{cases} -1. & \text{Do not search for shadow times} \\ \geq 0. & \text{Time in days from epoch to begin search for shadow times.} \end{cases}$

Built-in value is -1.

766 XNOR

Central body for initial input state vector

1. Earth
2. Moon
3. Sun
4. Venus
5. Mars
6. Jupiter

Built-in value is 1.

767 XNE

Error control for FNOL II. Controls the size of the automatic step calculated in FNOL II.
Built-in value is 5. May be as high as 9.
See reference 3 for details.

768 HARMONICS

Oblateness key in form of abc., where

a = Earth
b = Moon
c = Mars

0 Do not include oblateness
1 Include oblateness

Built-in value is 111. Only the central body oblateness is used.

769 SOLAR

Solar Pressure Key

0. Do not include solar pressure and ignore c(770) through c(774)
1. Include solar pressure

Built-in value is 0.

770	AREA	Cross sectional area of spacecraft in cm^2 . Built-in value is 22225. Used only if $c(769) = 1$.
771	XMASS	Total mass of spacecraft in gms. Built-in value is 113000. Used only if $c(769) = 1$.
772	Reflectivity of spacecraft	<div> <div> Values from 0. to 1., inclusive. Used only if $c(769) = 1$. </div> <div> 1. Perfect reflector 0. Perfect absorber Built-in value is 0.2 </div> </div>
773	SPEC. REFLECTION of spacecraft	<div> Fraction of particles specularly reflected. 1. 100% 0. 0% Built-in value is 1. May be 0. to 1., inclusive. Used only if $c(769) = 1$. </div>
774	CONSTANT	<div> Solar pressure at 1 A.U. Built-in value is 4.7×10^{-5} dynes/cm^2. Used only if $c(769) = 1$. </div>
775	INPUT TYPE	<div> 0. Cartesian. 1. Orbital elements. Built-in value is 0. Actual values are input through $c(750) - c(756)$. </div>
776	APPER	<div> Apoapsis and periapsis key. 0. Do not print at apoapsis or periapsis. 1. Print only at apoapsis. -1. Print only at periapsis. Built-in value is 0. </div>
777	OUTPUT =	<div> <div> Output options in form of abcdefgh. </div> <div> a: Central body mean Earth equator of 1950 b: Selenographic c: Mars mean equator of date d: Central body true ecliptic and equinox of date e: Earth-centered true ecliptic and equinox of date </div> </div>

- f: Sun-centered true ecliptic and equinox of date
 - g: Central body true Earth equator and equinox of date
 - h: Earth-fixed latitude and longitude (only if Earth is central body)
 - 0 Do not print this form.
 - 1 Print this form.
- Built-in value is 10000011.

Cases may be stacked. When this is desired, cards for the 1st case are followed by a blank card and then the cards for the second case. There is no limit to the number of cases that may be stacked. Again, since an overlay method is used on input, only those variables different from those for the preceding case need be input. A blank card at the end of the last case is necessary to end the program. A sample of the input is shown in Appendix B.

OUTPUT

The output options are listed above in the description of array c(777). TRIP has the capability of automatically switching body centers when the probe leaves the sphere of influence of one body and enters that of another body. This switching does not interfere with the printout options.

Printout for the central body consists of both the cartesian state vector and instantaneous osculating elements; for other bodies, only the state vector. A sample of the output with an explanation is shown in Appendix B.

CONSTANTS

All constants needed by TRIP are listed in subroutine KONSTK and are either described there by a comment card or are described above in the input section. The constants in c(31) through c(38) are no longer used by the program but were not taken out.

Any or all of these constants may be changed for a particular run by including the proper array number and the new value in the input data.

KNOWN RESTRICTIONS AND ANOMALIES

There are two restrictions to be noted in using TRIP:

- 1.) Only one type of printout can be used in a run.

2. The printout interval must be greater than two minutes which is the initial time step in the integrator. If a request for a smaller interval is made, the program automatically sets the printout interval to be slightly greater than 2 minutes and prints out a message to this effect.

There are also two known anomalies in the program, which cause inconvenience but do not produce incorrect results:

1. When periapsis printout is requested, occasionally the program will intersperse a printout at apoapsis and then continue with periapsis printouts. Similarly, a printout at periapsis may occur when printout is requested at apoapsis.
2. When shadow times are requested, if the satellite is already in shadow at the time the shadow search is initiated, the printout of the shadow time is incorrect for that shadow interval only. All subsequent printout are correct. This bug occurs because the search procedure used requires a point before shadow occurs in order to iterate to the correct time. These incorrect shadow times will be obvious to the user (see case 6, Appendix B).

A final note of caution — when exact printout is asked for, the numerical integrator must restart after each printout time in order to continue. This procedure may result in a loss of accuracy due to numerical problems; that is if 2 cases are stacked using the same trajectory, one asking for exact printout and the other asking for printout only at the last point, the final state vectors at the stop time may disagree somewhat. To a certain extent, the numerical errors may be minimized by increasing the size of the error col rol in array c(767) or by decreasing the rectification limit in array c(720). However this is a problem inherent to a certain extent in any numerical integration routine and probably can not be completely eliminated.

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3. Linnekin, J. S.; Belliveau, L. J., FNOL2, A Fortran (IBM 7090) Subroutine For the Solution of Ordinary Differential Equations with Automatic Adjustment of the Interval of Integration, NOLTR 63-171, Naval Ordnance Laboratory, White Oak, Maryland, 17 July 1963.
4. Hartwell, J. G., Lewis, T. R., Mathematical and Programming Documentation of a General Purpose Integrator Using Power Series Methods, NAS1-9389, DBA Systems, Inc., Melbourne, Florida, December, 1969.
5. Linnekin, J. S., DE-19* Direct Access Double Precision Ephemeris Package for the IBM 360/95, GSFC document X-551-69-375, September, 1969.

APPENDIX A

Listing of TRIP

C-----	ENCKE	PROGRAM	MAIN	100
	IMPLICIT	REAL	*R(A-H,O-Z,\$)	200
	DIMENSION	X(3),V(3),R1(3,8),V1(3,8)		300
	DIMENSION	DUM(3,3),DATEFC(3,3),DATECT(3,3),XX(3),XV(3)		400
	COMMON	C(1000),IC(50),Z(3),VV(3),NOR,INP		500
	DIMENSION	XNOT(3)		600
	DIMENSION	ELI(6)		700
	COMMON/APER/	FPROLD,OLD,XMAX		800
	COMMON/JTERM/	MEARTH,MMOON,MMARS		900
	DATA	BLK/6H /,XNOT1/3HNOT/		1000
	EQUIVALENCE	(C(401),R1(1,1)),(C(425),V1(1,1)),		1100
	1	(C(750),X(1)),(C(753),V(1))		1200
	DIMENSION	A(3,3),FN(3,3),EMN(3,3),DATE(3,3),SDATE(3,3),		1300
	1	DATET(3,3),SDATET(3,3),ADATE(3,3),ADATET(3,3),AR(3,3)		1400
	COMMON/ROT/	DATE,SDATE,DATET,SDATET,ADATE,ADATET,DATEFC,DATECT,EN		1500
	COMMON/XLIR/	SG,TA,XMLIR		1600
	COMMON/TUP/	TLU		1700
	COMMON /SHAD/	SHADK		1800
	COMMON/PRINT/	IC50,ISEL,MARDAT,ICFNEC,IFAREC,ISUNEC,ICDATE,IFARFX		1900
	CALL	KONSTK		2000
	1	CALL OVRLAY		2100
		C(462)=1.00		2200
		C(122)=1.00		2300
		FPROLD=0.00		2400
		OLD = 0.00		2500
		IF(C(775).EQ.0.00) GO TO 2		2600
		NTEMP=C(766)		2700
		DO 5 I=1,6		2800
5		ELI(I) = C(I+749)		2900
		CALL ORB2X(X,V,ELI,C(NTEMP))		3000
	2	CONTINUE		3100
		IF(FNORM(X).EQ.0.00) GO TO 20		3200
		SHADK=0.000		3300
		TS=C(756)		3400
		DF=C(757)		3500
		INP=C(758)		3600
		ST=C(759)		3700
		STF=C(760)		3800
		TINC=C(761)		3900
		TOTAL=C(762)		4000
		C(1000)=C(765)		4100
		XNOR=C(766)		4200
		NE=C(767)		4300
		MEARTH=C(768)/100.00		4400
		TEMP=C(768)-MEARTH*100		4500
		MMOON=TEMP/10.00		4600
		TEMP=TEMP-MMOON*10		4700
		MMARS=TEMP		4800
		IC50=C(777)/10000000.00		4900
		TEMP=C(777)-IC50*10000000		5000
		ISEL=TEMP/1000000.00		5100
		TEMP=TEMP-ISEL*1000000		5200
		MARDAT=TEMP/100000.00		5300
		TEMP=TEMP-MARDAT*100000		5400
		ICENEC=TEMP/10000.00		5500
		TEMP=TEMP-ICENEC*10000		5600
		IFAREC=TEMP/1000.00		5700
		TEMP=TEMP-IFAREC*1000		5800
		ISUNEC=TEMP/100.00		5900
		TEMP=TEMP-ISUNEC*100		6000
		ICDATE=TEMP/10.00		6100
		TEMP=TEMP-ICDATE*10		6200
		IFARFX=TEMP		6300
		NTOTAL=TOTAL		6400
		NOR=XNOR		6500
		CALL TIMEC(TS,DF,TW,TF)		6600
		CALL TIMEC(ST,STF,ST1,STF1)		6700

IF(C(1000)) 60,50,50	6800
60 WRITE(6,30)	6900
GO TO 70	7000
50 WRITE(6,40)	7100
40 FORMAT(1H1,19HSHADOW IS REQUESTED)	7200
30 FORMAT(1H1,23HSHADOW IS NOT REQUESTED)	7300
70 CONTINUE	7400
XNOT(1)=BLK	7500
XNOT(2)=HLK	7600
XNOT(3)=BLK	7700
IF(MEARTH.LT.1) XNOT(1)=XNOT1	7800
IF(MMOON.LT.1) XNOT(2)=XNOT1	7900
IF(MMARS.LT.1) XNOT(3)=XNOT1	8000
WRITE(6,100) C(61),XNOT(1)	8100
WRITE(6,100) C(62),XNOT(2)	8200
WRITE(6,100) C(65),XNOT(3)	8300
100 FORMAT(1H0,13HHARMONICS OF ,A6,4H IS ,A4,8HINCLUDED)	8400
XNOT(1)=BLK	8500
IF(C(769).EQ.0.000) XNOT(1)=XNOT1	8600
WRITE(6,102) XNOT(1)	8700
102 FORMAT('0 SOLAR RADIATION PRESSURE IS ',A4,' INCLUDED')	8800
TIME=TW+TF	8900
TLU=TIME	9000
CALL ROTEQ(TIME,A)	9100
CALL NUTAIT(TIME,OM,CR,DT,EN,EPSIL)	9200
CALL MNA(TIME,OM,CR,DT,EPSIL,RU,G,GP,WW,EMN)	9300
XMLIB=180.00*.0174532925200 + CR-OM+TA-SG	9400
CALL MULT(EN,A,DATE)	9500
DUM(1,1)=1.000	9600
DUM(1,2)=0.00	9700
DUM(1,3)=0.00	9800
DUM(2,1)=0.00	9900
DUM(2,2)=DCOS(EPSIL)	10000
DUM(2,3)=DSIN(EPSIL)	10100
DUM(3,1)=0.00	10200
DUM(3,2)=-DSIN(EPSIL)	10300
DUM(3,3)=DCOS(EPSIL)	10400
CALL MULT(DUM,DATE,DATEEC)	10500
CALL MULT(EMN,DATE,SDATE)	10600
CALL ARES(TS,DF,AR)	10700
CALL MULT(AR,A,ADATE)	10800
DO 101 I=1,3	10900
DO 101 J=1,3	11000
DATECT(J,I)=DATEEC(I,J)	11100
DATET(J,I)=DATE(I,J)	11200
SDATET(J,I)=SDATE(I,J)	11300
101 ADATET(J,I)=ADATE(I,J)	11400
WRITE(6,6)	11500
6 FORMAT(1H0,31HINPUT IN MEAN EQ AND EQ OF 1950)	11600
CALL DATOUT(TW,TF,DAYM,FDATE,0)	11700
DO 600 I=1,3	11800
XX(I)=X(I)	11900
600 XV(I)=V(I)	12000
GO TO(200,300,400,500,700),INP	12100
300 CALL M1(X,DATECT,XX)	12200
CALL M1(V,DATECT,XV)	12300
GO TO 200	12400
400 CALL M1(X,SDATET,XX)	12500
CALL M1(V,SDATET,XV)	12600
GO TO 200	12700
500 CALL M1(X,ADATET,XX)	12800
CALL M1(V,ADATET,XV)	12900
GO TO 200	13000
700 CALL M1(X,DATET,XX)	13100
CALL M1(V,DATET,XV)	13200
200 CONTINUE	13300

DO 11 I=1,3	13400
C(I+499)=XX(I)	13500
11 C(I+502)=XV(I)	13600
CALL OUTX(XX,XV,NOUT)	13700
C(592)=TW	13800
C(593)=TF	13900
TFF=TF	14000
KK=1	14100
13 TFF=TFF+TINC	14200
CALL TFRAC(TW,TFF,TWF,TFF)	14300
16 XMAX=0.00	14400
CALL TRAJ(TWF,TFF,XX,XV,NE)	14500
IF(C(462).EQ.0.00)GO TO 1	14600
TW=TWF	14700
DO 10 JJ=1,3	14800
C(JJ+499)=XX(JJ)	14900
10 C(JJ+502)=XV(JJ)	15000
STDT=(ST1-C(592)+STF1-C(593))*86400.00	15100
IF(STDT-120.00.LE.0.00) GO TO 1	15200
XMAX=0.00	15300
IF(C(1000).GT.0.00) C(1000)=0.00	15400
14 IF(C(462).EQ.0.00) GO TO 1	15500
IF(FPROLD.EQ.0.00) GO TO 12	15600
FPROLD=0.00	15700
OLD = 0.00	15800
STDTPR=(TWF-C(592)+TFF-C(593))*86400.00	15900
IF(STDTPR.LE.120.00) GO TO 12	16000
IF (KK .LE. NTOTAL) GO TO 16	16100
GO TO 15	16200
12 KK=KK+1	16300
15 IF(KK.LE.NTOTAL) GO TO 13	16400
CALL TRAJ(ST1,STF1,XX,XV,NE)	16500
IF(FPROLD.NE.0.00) GO TO 14	16600
GO TO 1	16700
20 CONTINUE	16800
STOP	16900
END	17000

	REAL FUNCTION ADOT*8(X,Y)	17100
	IMPLICIT REAL*8(A-H,O-Z,\$)	17200
	DIMENSION X(3), Y(3)	17300
C	FUNCTION RETURNS ANGLE IN DEGREES BETWEEN TWO INPUT VECTORS	17400
C	RANGE IS RESTRICTED TO (0,180)	17500
	A=FNORM(X)	17600
	B=FNORM(Y)	17700
	ANG=DOT(X,Y)/A/B	17800
	ADOT=ARKTNS(180,ANG,DSQRT(1.000-ANG*ANG))*57.29577900	17900
	RETURN	18000
	END	18100

SUBROUTINE ARES(T1,T2,AR)	18200
IMPLICIT REAL*8(A-H,O-Z,S)	18300
DIMENSION AR(3,3),EE(3),O(3),EXO(3),FO(3)	18400
DIMENSION TEM(3)	18500
DUM=0.00	18600
DTR=0.01745329252D0	18700
IYR=T1/100.00	18800
YR=IYR	18900
DT=YR-50.00	19000
AOP= 317.793416667D0+0.6520833D-2*DT	19100
DOP=54.6575D0+0.35D-2*DT	19200
BYR=YR*100.00+1.01D0	19300
CALL TIMEC(BYR,DUM,TW,TF)	19400
CALL TIMEC(T1,T2,TW1,TF1)	19500
TAU= ((TW1-TW)+(TF1-TF))/365.25D0	19600
AO= AOP-0.001013D0*TAU	19700
DO= DOP-0.000631D0*TAU	19800
TE= (TW1+TF1+18262.5D0)/36525.00	19900
OM= 48.78644167D0+0.77099167D0*TE-0.13888889D-5*TE*TE	20000
XI= 1.850333333D0-0.675D-3*TE+0.1261111D-4*TE*TE	20100
E= 23.45229444D0-0.130125D-1*TE-0.16388889D-5*TE*TE	20200
1 +0.50277778D-6*TE*TE*TE	20300
AOR=AO*DTR	20400
DOR= DO*DTR	20500
OMR= OM*DTR	20600
XIR= XI*DTR	20700
ER=E*DTR	20800
SAO=DSIN(AOR)	20900
CAO=DCOS(AOR)	21000
SDO=DSIN(DOR)	21100
CDO=DCOS(DOR)	21200
SOM=DSIN(OMR)	21300
COM=DCOS(OMR)	21400
SI=DSIN(XIR)	21500
CI=DCOS(XIR)	21600
SE=DSIN(ER)	21700
CE=DCOS(ER)	21800
C ***** THE FOLLOWING IS KAUFMAN'S METHOD *****	21900
EE(1)=CAO*CDO	22000
EE(2)=SAO*CDO	22100
EE(3)=SDO	22200
O(1)=SI*SOM	22300
O(2)= -SI*COM*CE-CI*SE	22400
O(3)= -SI*COM*SE+CI*CE	22500
CALL CROSS(O,EE,EXO)	22600
EQ(1)=-SAO	22700
EQ(2)=CAO	22800
EQ(3)=0.00	22900
CALL CROSS(EQ,EXO,TEM)	23000
SOMEG=DSORT(TEM(1)**2+TEM(2)**2+TEM(3)**2)	23100
COMEG= DOT(EQ,EXO)	23200
OMG=ARKTNS(180,COMEG,SOMEG)	23300
SOMEG=DSIN(OMG)	23400
COMEG=DCOS(OMG)	23500
AOM = AOR+1.570796327D0	23600
XAI=1.570796327D0-DOR	23700
SAOM=DSIN(AOM)	23800
CAOM=DCOS(AOM)	23900
SAI=DSIN(XAI)	24000
CAI=DCOS(XAI)	24100
AR(1,1)=COMEG*CAOM-SOMEG*SAOM*CAI	24200
AR(1,2)=COMEG*SAOM+SOMEG*CAOM*CAI	24300
AR(1,3)=SOMEG*SAI	24400
AR(2,1)=-SOMEG*CAOM-COMEG*SAOM*CAI	24500
AR(2,2)=-SOMEG*SAOM+COMEG*CAOM*CAI	24600
AR(2,3)=COMEG*SAI	24700
AR(3,1)=SAOM*SAI	24800

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AR(3,2)=-CAOM*SAI  
AR(3,3)=CAI  
RETURN  
END
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24900  
25000  
25100  
25200
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	REAL FUNCTION ARKTNS*(N,X,Y)	25300
	IMPLICIT REAL*(A-H,O-Z,S)	25400
C	COMPUTES 4-QUADRANT ARCTANGENT OF Y/X IN RADIANS	25500
C	N=360 ANGLE LIES IN RANGE (0,360) DEG	25600
C	N=180 ANGLE LIES IN RANGE (-180,180) DEG	25700
	TPI = 6.283185300000	25800
	XA = DABS(X)	25900
	YA = DABS(Y)	26000
	IF(XA-YA)1,1,2	26100
1	Z=X/YA	26200
	GO TO 3	26300
2	Z=Y/XA	26400
	YA=XA	26500
3	D=DSQRT(1.000+Z*Z)	26600
	YA=YA*D+X	26700
	IF(YA)4,4,5	26800
4	ARKTNS=TPI/2.000	26900
	GO TO 6	27000
5	ARKTNS=2.000*DATAN(Y/YA)	27100
6	IF(N-180)7,9,7	27200
7	IF(ARKTNS)8,9,9	27300
8	ARKTNS=ARKTNS+TPI	27400
9	RETURN	27500
	END	27600

	SUBROUTINE CROSS(A,B,C)	27700
	IMPLICIT REAL*8(A-H,O-Z,\$)	27800
	DIMENSION A(3),B(3),C(3)	27900
C	DIMENSION A(3),B(3),C(3)	28000
	C(1)=A(2)*B(3)-A(3)*B(2)	28100
	C(2)=A(3)*B(1)-A(1)*B(3)	28200
	C(3)=A(1)*B(2)-A(2)*B(1)	28300
	RETURN	28400
	END	28500

	SUBROUTINE DATOUT(T1,T2,DATE,FDATE,KDATE)	28600
	IMPLICIT REAL*8(A-H,O-Z,\$)	28700
C	DATE RETURNED IN FORMAT(YEARS FROM 1900)(MONTH).(DAYS)	28800
C	FDATE RETURNED IN FORMAT (HOURS)(MIN).(SECONDS)	28900
C	K SET 0 FOR PRINTOUT, SET - OR + FOR NO OUTPUT	29000
C	GIVES CALENDER DATE FROM T1(WHOLE DAYS FROM 1950)	29100
C	ANDT2(FRACT OF DAY)	29200
	DIMENSION C(12)	29300
C	DIMENSION C(12)	29400
	DATA Q000HL/6H JAN./	29500
	C(1)=Q000HL	29600
	DATA Q001HL/6H FEB./	29700
	C(2)=Q001HL	29800
	DATA Q002HL/6H MARCH/	29900
	C(3)=Q002HL	30000
	DATA Q003HL/6H APRIL/	30100
	C(4)=Q003HL	30200
	DATA Q004HL/6H MAY/	30300
	C(5)=Q004HL	30400
	DATA Q005HL/6H JUNE/	30500
	C(6)=Q005HL	30600
	DATA Q006HL/6H JULY/	30700
	C(7)=Q006HL	30800
	DATA Q007HL/6H AUG./	30900
	C(8)=Q007HL	31000
	DATA Q008HL/6H SEPT./	31100
	C(9)=Q008HL	31200
	DATA Q009HL/6H OCT./	31300
	C(10)=Q009HL	31400
	DATA Q010HL/6H NOV./	31500
	C(11)=Q010HL	31600
	DATA Q011HL/6H DEC./	31700
	C(12)=Q011HL	31800
	MD=0	31900
	K=T1+365.000	32000
	IF(T1)6,6,7	32100
6	WRITE (6,100)	32200
8	RETURN	32300
100	FORMAT(23H DATE IS 1950 OR BEFORE)	32400
7	K1=K/1461	32500
	K2=K-K1*1461	32600
	KWN=K2/365	32700
	KK=K1*4+1949+KWN	32800
	N=1	32900
	IF(KWN-3)112,111,111	33000
111	N=0	33100
112	KWN=K2-KWN*365	33200
	IF(KWN)11,11,13	33300
11	MONTH=1	33400
	MD=1	33500
	GO TO 25	33600
13	CONTINUE	33700
	KNW=0	33800
	JJ=0	33900
135	JJ=JJ+1	34000
	IF(12-JJ)23,23,137	34100
C	J,F,M,A,M,J,J,A,S,O,N,MONTHS FOR GO TO	34200
137	GO TO (14,15,14,16,14,16,14,14,16,14,16,14),JJ	34300
14	CONTINUE	34400
	KNW=KNW+31	34500
	GO TO 17	34600
15	CONTINUE	34700
	IF(N)18,18,19	34800
18	KNW=KNW+1	34900
19	KNW=KNW+28	35000
	GO TO 17	35100
16	KNW=KNW+30	35200

17	CONTINUE	35300
	IF(KWN-KNW)20,21,22	35400
22	CONTINUE	35500
	MD=KNW	35600
	GO TO 135	35700
20	CONTINUE	35800
	MONTH=JJ	35900
	MD=KWN-MD+1	36000
	GO TO 25	36100
21	CONTINUE	36200
	MONTH=JJ+1	36300
	MD=1	36400
	GO TO 25	36500
23	MONTH=12	36600
	MD=KWN-MD+1	36700
25	CONTINUE	36800
	TH=T2*24.000	36900
	THP=IDINT(TH)	37000
	FDATE=THP*100.000	37100
	NHOUR=THP	37200
	THP=(TH-THP)*60.000	37300
	TH=IDINT(THP)	37400
	FDATE=FDATE+TH	37500
	NMIN=TH	37600
	THP=(THP-TH)*60.000	37700
	NSEC=THP	37800
	FDATE=FDATE+THP/100.000	37900
	TSEC=NSEC	38000
	DATE=(KK-1900)*100+MONTH	38100
	SP=MD	38200
	DATE=DATE+SP/100.000	38300
	IF(KDATE) 8,50,8	38400
50	CONTINUE	38500
	THP=(THP-TSEC)*1000.000	38600
	NFSEC=THP	38700
	TT=IDINT(T2+.500)	38800
	TP2=T2+.500-TT	38900
	TP1=T1+TT+2433282.000	39000
	WRITE (6,101)C(MONTH),MD,KK,NHOUR,NMIN,NSEC ,NFSEC,TP1,TP2	39100
101	FORMAT(1H ,A6,I3,1H,,1X,I4,1H ,1X,I2,4HHR\$, ,I3,4HMIN, ,I3,1H, ,I3,	39200
	13HSEC,50X,12HJULIAN DATE ,F8.0,T111,F9.8)	39300
	GO TO 8	39400
	END	39500

SUBROUTINE DERIV(X,Y,D)	39600
IMPLICIT REAL*8(A-H,O-Z,\$)	39700
DIMENSION Y(20),R1(3,8),V1(3,8),D(20),CR(20),NP(5), RM(5),RM1(5),	39800
1 DACC(3),Z1(3),VV1(3),RE(3),CACC(3) ,R2(3,8)	39900
DIMENSION DACC(3)	40000
DIMENSION SACC(3)	40100
COMMON C(1000),IC(50),Z(3),VV(3),NOR	40200
COMMON/JTERM/MEARTH,MMOON,MMARS	40300
COMMON/DISTRB/DACC,CACC,DACC	40400
COMMON /SHAD/SHADK	40500
EQUIVALENCE (C(401),R1(1,1)),(C(425),V1(1,1))	40600
C MUST CALCULATE POSITION OF PROBE FROM INCREMENTS	40700
DT=X	40800
I=C(NOR)	40900
IF(X.NE.0.00) GO TO 321	41000
DO 322 I=1,3	41100
Z(I)=C(I+499)	41200
322 VV(I)=C(I+502)	41300
GO TO 323	41400
321 CONTINUE	41500
MN=1	41600
CALL STEPD(MN,DT,TA,C(500),C(503),U,Z,VV,1,CR)	41700
323 CONTINUE	41800
DO 10 I=1,3	41900
Z1(I)=Z(I)+Y(I)	42000
10 VV1(I)=VV(I)+Y(I+3)	42100
TW=C(592)	42200
TF=C(593)+(C(719)+C(506)+X)/86400.00	42300
CALL TFRAC(TW,TF,TW,TF)	42400
CALL SHIFTP(NOR,Z1,VV1,TW,TF,R1,V1)	42500
NP(1)=2	42600
NP(2)=3	42700
NP(3)=4	42800
NP(4)=5	42900
NP(5)=6	43000
GO TO(1,2,3,90,80,100),NOR	43100
2 NP(1)=1	43200
GO TO 1	43300
3 NP(2)=1	43400
GO TO 1	43500
90 NP(3)=1	43600
GO TO 1	43700
80 NP(4)=1	43800
GO TO 1	43900
100 NP(5)=1	44000
GO TO 1	44100
1 CONTINUE	44200
DO 4 I=1,5	44300
NP1=NP(I)	44400
RM(I)=FNORM(R1(I,NP1))**3	44500
DO 5 J=1,3	44600
5 R2(J,I+3)=R1(J,NOR)-R1(J,NP1)	44700
4 RM1(I)=FNORM(R2(I,I+3))**3	44800
NP1=NP(1)	44900
NP2=NP(2)	45000
NP3=NP(3)	45100
NP4=NP(4)	45200
NP5=NP(5)	45300
DO 6 I=1,3	45400
6 DACC(I)=-C(NP1)*(R1(I,NP1)/RM(1)+R2(I,4)/RM1(1))-C(NP2)*(R1(I,NP2)	45500
1/RM(2)+R2(I,5)/RM1(2))	45600
2-C(NP3)*(R1(I,NP3)/RM(3)+R2(I,6)/RM1(3))-C(NP4)*(R1(I,NP4)	45700
3/RM(4) +R2(I,7) /RM1(4))-C(NP5)*(R1(I,NP5)/RM(5)+R2(I,8)/RM1(5))	45800
DO 7 I=1,3	45900
7 RE(I)=Z1(I)+.500*Y(I)	46000
Q= DOT(RE,Y)/(FNORM(Z)**2)	46100
SUM =1.00	46200

TERM=1.00	46300
DO 8 K=2,50	46400
XK=K	46500
TERM=TERM*((.500-XK)*2.00*Q/(XK-1.00))	46600
SUM=SUM+TERM	46700
IF(DABS(TERM).LT.0.0000100*SUM) GO TO 9	46800
8 CONTINUE	46900
WRITE(6,20)	47000
20 FORMAT(1H1,34H0 SERIES IN ENCKE DID NOT CONVERGE)	47100
STOP	47200
9 FQ=1.00-SUM	47300
H=C(NOR)/(FNORM(Z)**3)	47400
DO 11 I=1,3	47500
11 CACC(I)=-H*Y(I)+H*FQ*R1(I,NOR)	47600
DO 30 I=1,3	47700
30 OACC(I)=0.00	47800
GO TO (40,50,21,21,60,21),NOR	47900
40 IF(MEARTH.NE.1) GO TO 21	48000
GO TO 70	48100
50 IF(MMOON.NE.1) GO TO 21	48200
GO TO 70	48300
60 IF(MMARS.NE.1) GO TO 21	48400
70 CONTINUE	48500
TWTE=C(592)	48600
TFTE=C(593)+(C(506)+X)/86400.00	48700
CALL TFRAC(TWTE,TFTE,TWTE,TFTE)	48800
TIMUP=TWTE+TFTE	48900
CALL HARMON(R1,V1,OACC,TIMUP)	49000
21 CONTINUE	49100
DO 13 I=1,3	49200
13 DACC(I)=DACC(I)+OACC(I)	49300
RAT = FNORM(Y(1)) / FNORM(Z(1))	49400
IF(RAT.GE.C(720).OR.0.GE.C(720)) C(122)=0.000	49500
DO 17 I=1,3	49600
17 OACC(I)=OACC(I)+CACC(I)	49700
IF(C(769).EQ.0.000.OR.SHADK.EQ.1.000) GO TO 551	49800
C* * * * * CALCULATE SOLAR PRESSURE * * * * *	49900
CALL SOLAR(R1(1,3),SACC)	50000
DO 1000 I=1,3	50100
1000 OACC(I)=OACC(I) + SACC(I)	50200
551 C O N T I N U E	50300
DO 16 I=1,3	50400
D(I)=Y(I+3)	50500
16 D(I+3)=OACC(I)	50600
RETURN	50700
END	50800

	REAL FUNCTION DOT*8(X,Y)	50900
	IMPLICIT REAL*8(A-H,O-Z,\$)	51000
	DIMENSION X(3),Y(3)	51100
C	DIMENSION X(3),Y(3)	51200
	DOT = X(1)*Y(1) + X(2)*Y(2) + X(3)*Y(3)	51300
	RETURN	51400
	END	51500

	SUBROUTINE FNOL2(J,N,G,L,M,NE,X,Y,D,DD,TT,QQ)	51600
	IMPLICIT REAL*8(A-H,O-Z,S)	51700
	COMMON BERNIE(1000)	51800
C		51900
C		52000
	DOUBLE PRECISION XD,YD,YA,YC,YP,YI	52100
C	DIMENSION Y(50),D(50),YB(30,6),GI2(30),GI3(30),GI4(30),EF(30),	52200
	DIMENSION Y(8000)	52300
	DIMENSION ZZ(5),D(50),YB(30,6),GI2(30),GI3(30),GI4(30),EF(30),	52400
	1EF1(30),EF2(30),EF3(30),YI(30),ERROR(30),HA(30),YA(50),DA(50),	52500
	2YC(30),YP(30),YD(50)	52600
	EC=Y(N+3)	52700
9876	FORMAT(1H0,I7)	52800
	1 H=G	52900
	2 HZ=H	53000
	3 LN=N+MAX0(L,3)	53100
C	SUBROUTINE FNOL2(J,N,G,L,M,NE,X,Y,D,DERIV,TERM,OUT)	53200
6876	FORMAT(1H0,I7)	53300
	4 NA=0	53400
	5 NB=1	53500
	6 NF=0	53600
	7 NG=0	53700
	8 F=0.00	53800
	9 FA=0.00	53900
	10 FB=0.00	54000
	11 FC=0.00	54100
	12 CONTINUE	54200
	13 ENE=NE	54300
C	DO 200 I=1,LN	54400
C 200	YD(I)=DBLE(Y(I))	54500
C	XD=DBLE(X)	54600
	DO 200 I=1,LN	54700
200	YD(I)=Y(I)	54800
	XD=X	54900
	14 IF(J-3)15,21,15	55000
	15 IF(NE)18,16,18	55100
	16 JA=4	55200
	17 GO TO 22	55300
	18 RE1=10.00**(-ENE)	55400
	19 RE2=10.00**(-ENE-3.000)	55500
	20 REM=10.00**(-ENE-1.500)	55600
	21 JA=1	55700
	22 DO 25 I=1,N	55800
	23 DO 24 IC=1,5	55900
	24 YB(I,IC)=0.00	56000
	25 ERROR(I)=0.00	56100
	26 CALL DERIV(X,Y,D)	56200
	CALL TERM(X,Y,D,F)	56300
	IF(DABS(F)-1.00-9) 731,731,5209	56400
5209	CONTINUE	56500
	DO 300 I=1,N	56600
	GI2(I)=D(I)	56700
	GI3(I)=D(I)	56800
	GI4(I)=D(I)	56900
300	EF(I)=D(I)	57000
C 27	CALL OUTPUT(X,Y,D,ERROR,N,L,H)	57100
27	CALL OUT(X,Y,D,ERROR,N,L,H)	57200
	IF(BERNIE(506).NE.0.00) GO TO 29	57300
	28 FD=Y(N+1)	57400
	29 IF(J-2) 30,129,30	57500
	30 GO TO(31,37,35,37),JA	57600
	31 DO 33 I=1,LN	57700
	32 YA(I)=YD(I)	57800
	33 DA(I)=D(I)	57900
	34 GO TO 37	58000
	35 H8=H	58100
	36 H=2.00*H	58200

37	HD2 = .500*H	58300
	DO 39 I=1,N	58400
38	YB(I,NB)=D(I)	58500
	XL = D(I) * HD2	58600
C 39	Y(I)=SNGL(YD(I)+XL)	58700
39	Y(I)=YD(I)+XL	58800
C	X=SNGL(XD+HD2)	58900
	X=XD+HD2	59000
40	CALL DERIV (X,Y,G12)	59100
41	DO 42 I=1,N	59200
	XL = G12(I)*HD2	59300
C 42	Y(I)=SNGL(YD(I)+XL)	59400
42	Y(I)=YD(I)+XL	59500
43	CALL DERIV (X,Y,G13)	59600
44	DO 45 I=1,N	59700
	XL=G13(I)*H	59800
C 45	Y(I)=SNGL(YD(I)+XL)	59900
45	Y(I)=YD(I)+XL	60000
C	X=SNGL(XD+H)	60100
	X=XD+H	60200
46	CALL DERIV(X,Y,G14)	60300
47	HD6 =H/6.DO	60400
	GO TO(48,55,60,66),JA	60500
48	DO 52 I=1,N	60600
	XL=(D(I) + 2.DO*(G12(I) + G13(I)) +G14(I))*HD6	60700
49	YC(I)=YD(I)+XL	60800
51	YD(I)=YA(I)	60900
52	ERROR(I)=0.DO	61000
53	JA=3	61100
54	GO TO 35	61200
55	DO 57 I=1,N	61300
	XL=(D(I) + 2.DO*(G12(I) + G13(I)) +G14(I))*HD6	61400
56	YD(I)=YD(I)+XL	61500
C 57	ERROR(I)=SNGL(YD(I)-YP(I))/15.	61600
57	ERROR(I)=(YD(I)-YP(I))/15.DO	61700
58	JA=1	61800
59	GO TO 681	61900
60	DO 62 I=1,N	62000
61	YD(I)=YC(I)	62100
	XL=(D(I) + 2.DO*(G12(I) + G13(I)) +G14(I))*HD6	62200
62	YP(I)=YA(I)+XL	62300
63	H=HB	62400
64	JA=2	62500
65	GO TO 681	62600
66	DO 68 I=1,N	62700
	XL=(D(I) + 2.DO*(G12(I) + G13(I)) +G14(I))*HD6	62800
67	YD(I)=YD(I)+XL	62900
68	ERROR(I)=0.DO	63000
681	DO 69 I=1,N	63100
C 69	Y(I)=SNGL(YD(I))	63200
69	Y(I)=YD(I)	63300
	XD=XD+H	63400
C	X=SNGL(XD)	63500
	X=XD	63600
70	CALL DERIV(X,Y,D)	63700
71	FC=F	63800
72	CALL TERM(X,Y,D,F)	63900
73	IF(DABS(F)-1.00-9)731,731,733	64000
731	NF=5	64100
732	GO TO 124	64200
733	IF(F)74,124,76	64300
74	FA=1.00	64400
75	GO TO 77	64500
76	FB=1.00	64600
77	IF(FA-FB)83,78,83	64700
78	NF=NF+1	64800

79	JA=4	64900
80	NB=1	65000
81	H=H*F/(FC-F)	65100
82	IF(NF-4)37,37,124	65200
83	IF(NE)84,117,84	65300
84	IF(JA-1)117,85,117	65400
85	IF(J-3)86,117,86	65500
86	DO 95 I=1,N	65600
	IF(Y(I))886,885,886	65700
885	HA(I)=1000.00	65800
	GO TO 95	65900
886	IF(EC)880,890,87	66000
87	IF(DABS(Y(I))-EC) 880,880,890	66100
880	IF(DABS(ERROR(I))-RE2) 882,94,881	66200
881	IF(DABS(ERROR(I))-RE1)94,94,882	66300
882	HA(I)=H*(REM/(DABS(ERROR(I))+.000000000100))*(.200)	66400
883	GO TO 95	66500
890	IF(DABS(ERROR(I)/Y(I))-RE2)892,94,891	66600
891	IF(DABS(ERROR(I)/Y(I))-RE1)94,94,892	66700
892	HA(I)=H*(REM/(DABS(ERROR(I)/Y(I))+.000000000100))*(.200)	66800
893	GO TO 95	66900
94	HA(I)=H	67000
95	CONTINUE	67100
96	HB=DABS(HA(N))	67200
97	DO 98 I=1,N	67300
C 98	HB=AMIN1(ABS(HA(I)),HB)	67400
98	HB=OMIN1(DABS(HA(I)),HB)	67500
99	IF(DABS(H)-HB)100,117,101	67600
100	IF(DABS(HZ)-DABS(H))101,101,116	67700
101	DO 103 I=1,LN	67800
102	YD(I)=YA(I)	67900
C	Y(I)=SNGL(YD(I))	68000
	Y(I)=YD(I)	68100
103	D(I)=DA(I)	68200
104	IF(NB-6) 107,105,105	68300
105	XD=XD-H	68400
106	GO TO 109	68500
107	XD=XD-2.00*H	68600
108	HZ=H	68700
109	H=DSIGN(HB,H)	68800
	X=XD	68900
C	X=SNGL(XD)	69000
	CALL DERIV(X,Y,D)	69100
	CALL TERM(X,Y,D,F)	69200
110	NB=1	69300
111	XABS=DABS(.00000100*X)	69400
112	IF(DABS(H)-XABS)113,113,117	69500
113	NG=NG+1	69600
114	H=DSIGN(XABS,H)	69700
115	IF(NG - 10)124,150,150	69800
150	WRITE(6,1261) H	69900
1261	FORMAT (1H1,107HEXECUTION TERMINATED BECAUSE INTERVAL OF INTEGRATI	70000
	ION LESS THAN 1.0E -6 TIMES INDEPENDENT VARIABLE (X). X =,1PD15.7)	70100
	STOP	70200
116	HZ=H	70300
117	IF(N)118,118,121	70400
118	IF(DABS(Y(N+1)-FD)-Y(N+2))29,119,119	70500
119	FD=FD+Y(N+2)	70600
120	GO TO 124	70700
121	NA=NA+1	70800
122	IF(N-NA)123,123,29	70900
123	NA=0	71000
C124	CALL OUTPUT(X,Y,D,ERROR,N,L,H)	71100
124	CALL OUT(X,Y,D,ERROR,N,L,H)	71200
125	IF(NF-4)29,29,126	71300
126	CONTINUE	71400

128 RETURN	71500
129 NB=NB+1	71600
130 IF(NB-6)30,131,136	71700
131 DO 134 I=1,N	71800
132 EF3(I)=YB(I,3)	71900
133 EF2(I)=YB(I,4)	72000
134 EF1(I)=YB(I,5)	72100
135 GO TO 137	72200
136 NB=10	72300
137 HD24 =H/24.DO	72400
DO 138 I=1,N	72500
XL =(55.DO*D(I) -59.DO*EF1(I) +37.DO*EF2(I) -9.DO*EF3(I))*HD24	72600
YP(I)=YD(I)+XL	72700
C 138 Y(I)=SNGL(YP(I))	72800
C X=SNGL(XD+H)	72900
138 Y(I)=YP(I)	73000
X=XD+H	73100
139 CALL DERIV(X,Y,EF)	73200
140 DO 142 I=1,LN	73300
141 YA(I)=YD(I)	73400
142 DA(I)=D(I)	73500
143 DO 148 I=1,N	73600
XL =(9.DO*EF(I) +19.DO*D(I) -5.DO*EF1(I) +EF2(I))*HD24	73700
144 YD(I)=YD(I)+XL	73800
C 145 ERROR(I)=-SNGL(YD(I)-YP(I))/14.	73900
145 ERROR(I)=-{YD(I)-YP(I)}/14.DO	74000
146 EF3(I)=EF2(I)	74100
147 EF2(I)=EF1(I)	74200
148 EF1(I)=D(I)	74300
999 CONTINUE	74400
149 GO TO 681	74500
END	74600

	REAL FUNCTION FNORM*8(X)	74700
	IMPLICIT REAL*8(A-H,O-Z,S)	74800
	DIMENSION X(3)	74900
C	DIMENSION X(3)	75000
	1 FNORM=DSORT(X(1)**2+X(2)**2+X(3)**2)	75100
	3 RETURN	75200
	END	75300

SUBROUTINE GETACC (LCT, ICT, CNM, SNM, ECN, PVA, CTT, CTB, UMT, VMT, NTE)	75400
IMPLICIT REAL*8(A-H, O-Z, S)	75500
DIMENSION LCT(1), ICT(1), CNM(1), SNM(1), ECN(1)	75600
DIMENSION PVA(1), CTT(1), CTB(1), UMT(1), VMT(1)	75700
EQUIVALENCE (XP, PX), (YP, PY), (ZP, PZ)	75800
ERD=ECN(1)	75900
XMU=ECN(2)	76000
ALF=ECN(3)	76100
PX= PVA(1)	76200
PY= PVA(2)	76300
PZ= PVA(3)	76400
CGB=DCOS(ALF)	76500
SGB=DSIN(ALF)	76600
RMT=1.000/(PX*PX+PY*PY+PZ*PZ)	76700
TMA=RMT*ERD	76800
CLT=TMA*(XP*CGB+YP*SGB)	76900
SLT=TMA*(YP*CGB-XP*SGB)	77000
RZR=TMA*ZP	77100
RMR=TMA*ERD	77200
TWR=0.500/ERD	77300
RMO=DSQRT(RMT)	77400
LMX=0	77500
LNC=1	77600
LA=LCT(2)	77700
IF (NTE-1) 15, 15, 20	77800
15 LA=0	77900
20 LB=LCT(1)	78000
LC=LA	78100
NB=NTE+1	78200
DO 75 I=1, NB	78300
KA=LA-1	78400
KB=LB	78500
KC=LC+1	78600
IF (KB-KA) 30, 35, 35	78700
30 KB=KA	78800
35 IF (LC) 50, 50, 40	78900
40 IF (KB-KC) 45, 50, 50	79000
45 KB=KC	79100
50 LNC=LNC+KB+1	79200
ICT(I)=LNC	79300
LA=LB	79400
LB=LC	79500
LC=LCT(I+2)	79600
IF (LMX-LA) 60, 65, 65	79700
60 LMX=LA	79800
65 IF (I-NTE+1) 75, 70, 70	79900
70 LC=0	80000
75 CONTINUE	80100
TMA=2.000	80200
TMB=2.000	80300
DO 90 I=1, LMX	80400
CTT(I)=-TMA	80500
CTB(I)= TMB	80600
TMA=TMA+2.000	80700
TMB=TMB+TMA	80800
90 CONTINUE	80900
UMT(1)=XMU*RMO	81000
VMT(1)=0.000	81100
LA=1	81200
LB=1	81300
NA=2	81400
KB=2	81500
DO 160 I=1, NB	81600
KC=ICT(I)-1	81700
KA=I-1	81800
TMB=KA+KA	81900

TMA=TMB+1.000	82000
TMC=1.000	82100
IF (KC-KB)140,100,100	82200
100 DO 130 LC=KB,KC	82300
TMD=RZR*UMT(LB)*TMA	82400
TME=RZR*VMT(LB)*TMA	82500
IF (KB-LC)110,120,120	82600
110 TMD=TMD-RMR*UMT(LB-1)*TMB	82700
TME=TME-RMR*VMT(LB-1)*TMB	82800
120 UMT(NA)=TMD/TMC	82900
VMT(NA)=TME/TMC	83000
TMA=TMA+2.000	83100
TMB=TMB+1.000	83200
TMC=TMC+1.000	83300
NA=NA+1	83400
130 LB=LB+1	83500
140 IF (I-NB)150,160,160	83600
150 TMC=KA+KA+1	83700
UMT(NA)=TMC*(CLT*UMT(LA)-SLT*VMT(LA))	83800
VMT(NA)=TMC*(CLT*VMT(LA)+SLT*UMT(LA))	83900
NA=NA+1	84000
KB=KC+2	84100
LB=LB+1	84200
LA=LB	84300
160 CONTINUE	84400
TMA=0.000	84500
TMB=0.000	84600
TMC=0.000	84700
TMD=0.500	84800
KB=1	84900
LA=ICT(1)	85000
LB=2	85100
LC=LA	85200
DO 260 I=1,NTE	85300
KC=LCT(I)	85400
IF (KC)260,260,210	85500
210 IF (I-2)230,215,220	85600
215 LA=3	85700
GO TO 225	85800
220 LA=ICT(I-2)+2	85900
225 LB=ICT(I-1)+1	86000
LC=ICT(I)	86100
230 DO 250 NA=1,KC	86200
TME=CTB(NA)	86300
TMF=TME	86400
IF (I-1)235,235,240	86500
235 TMF=TMD*TME	86600
TME=NA	86700
TMD=TMD*TME	86800
TME=NA+2	86900
TMD=TMD/TME	87000
TME=-TMF	87100
240 RMR=TME*UMT(LA)	87200
RZR=TMF*VMT(LA)	87300
CLT=UMT(LC)	87400
SLT=VMT(LC)	87500
TME=RMR-CLT	87600
TMF=RZR+SLT	87700
RMR=RMR+CLT	87800
RZR=RZR-SLT	87900
CLT=CNM(KB)	88000
SLT=SNM(KB)	88100
TMA=TMA+CLT*TME+SLT*RZR	88200
TMB=TMB-CLT*TMF+SLT*RMR	88300
TMC=TMC+CTT(NA)*(CLT*UMT(LB)+SLT*VMT(LB))	88400
LA=LA+1	88500

	LB=LB+1	88600
	LC=LC+1	88700
250	KB=KB+1	88800
260	CONTINUE	88900
	TMA=TMA*TWR	89000
	TMB=TMB*TWR	89100
	PVA(7)=(CGB*TMA-SGB*TMB)	89200
	PVA(8)=(SGB*TMA+CGB*TMB)	89300
	PVA(9)=TMC*TWR	89400
	RETURN	89500
	END	89600

	SUBROUTINE GETTAP	89700
	DEFINE FILE 10(958,6636,L,IV)	89800
	DOUBLE PRECISION TAB3,JD1,JDF,JD1,TDAY,JDIF,JDP	89900
	REAL NUTAT	90000
	REAL*8 TAB31	90100
	COMMON/CETBL2/ICW,ICENT,IREQ(13)	90200
	COMMON/CETBL3/TAB3(829),NUTAT(204),CKSUM	90300
	COMMON/CETBL9/JD1,TDAY,JDIF,IERR1	90400
	DATA IV/0/	90500
	DATA IWPRV/0/	90600
	JDP=JD1+TDAY	90700
	IF(JDP.LT.2438760.5D0.OR.JDP.GT.2446424.5D0)GO TO 100	90800
	IERR1=0	90900
	IF(ICW.NE.1) GO TO 205	91000
	DO 333 J=1,204	91100
333	NUTAT(J)=0.	91200
	ICW=2	91300
	IW=1	91400
	READ(10*IW)TAB3	91500
	TAB31=TAB3(1)	91600
205	IW=IDINT((JDP-TAB31)/8.D0)+1.D0	91700
	IF(IW.EQ.IWPRV)GO TO 220	91800
	IWPRV=IW	91900
200	READ(10*IW)TAB3	92000
	IF(JDP-TAB3(1))210,220,230	92100
210	IW=IW-2	92200
	GO TO 200	92300
230	IW=IW+1	92400
	IF(JDP-(TAB3(1)+8.D0))220,200,200	92500
220	JDIF=JDP-TAB3(1)	92600
	RETURN	92700
101	FORMAT(' EPHemeris ERROR--JULIAN DATE ',D25.7,' IS BEFORE JAN 1965	92800
	10R AFTER DEC 1985')	92900
100	WRITE(6,101)JDP	93000
	STOP	93100
	END	93200

SUBROUTINE GHA(TSEC,D,GHAN,DA,OMEGA)	93300
IMPLICIT REAL*8(A-H,O-Z)	93400
OMEGA=.0041780742D0/(1.D0+5.21D-13*D)	93500
DD=0.D0	93600
DD=0	93700
DD=DD*(.98564735D0/360.D0)	93800
DX=IDINT(DD)	93900
DD=DD-DX	94000
DF=DD	94100
TEM1=100.07554D0+360.D0*DF+2.9015D-13*D*D	94200
1+OMEGA*TSEC	94300
1 IF(TEM1)2,3,3	94400
2 TEM1=TEM1+360.D0	94500
GO TO 1	94600
3 IF(TEM1-360.D0)5,4,4	94700
4 TEM1=TEM1-360.D0	94800
GO TO 3	94900
5 GHAN=TEM1+DA*57.2957795D0	95000
RETURN	95100
END	95200

	SUBROUTINE GOTOR(K,VM,C,F,E1)	95300
	IMPLICIT REAL*8(A-H,O-Z,S)	95400
	DIMENSION C(2),F(4)	95500
C	DIMENSION C(2),F(4)	95600
C		95700
C		95800
C		95900
C		96000
	NMAX=20	96100
	N=0	96200
	GO TO (1,2),K	96300
1	CONTINUE	96400
C	FIRST GUESS IS OBTAINED FOR ELLIPTICAL CASE	96500
8	CONTINUE	96600
	IF(E1-1.0D0)30,31,31	96700
30	CONTINUE	96800
	D2=E1*E1	96900
	F(1)=E1*D2*(.16666667D+00-D2*(.83333333D-02-D2*(.198412698D-03-D2	97000
	1*(.275573192D-05-D2*.250521083D-07))))	97100
	F(2)=D2*(.5D0-D2*(.41666667D-01-D2*(.13888889D-02-D2*(.24801587D-0	97200
	14-D2*.27557319D-06))))	97300
	F(3)=E1-F(1)	97400
	F(4)=1.0D0-F(2)	97500
	GO TO 3	97600
31	CONTINUE	97700
	F(3)=DSIN(E1)	97800
	F(4)=DCOS(E1)	97900
	F(1)=E1-F(3)	98000
	F(2)=1.0D0-F(4)	98100
	GO TO 3	98200
2	CONTINUE	98300
C	FIRST GUESS IS OBTAINED FOR HYPERBOLIC CASE	98400
9	CONTINUE	98500
	IF(E1-1.0D0)32,33,33	98600
32	CONTINUE	98700
	D2=E1*E1	98800
	F(1)=E1*D2*(.16666667D+00+D2*(.83333333D-02+D2*(.198412698D-03+D2	98900
	1*(.275573192D-05+D2*.250521083D-07))))	99000
	F(2)=D2*(0.5D0+D2*(.41666667D-01+D2*(.13888889D-02+D2*(.24801587D-	99100
	104+D2*.27557319D-06))))	99200
	F(3)=E1+F(1)	99300
	F(4)=1.0D0+F(2)	99400
	GO TO 3	99500
33	CONTINUE	99600
	EX=.5D0*DEXP(E1)	99700
	OX=.25D0/EX	99800
	F(3)=EX-OX	99900
	F(4)=EX+OX	100000
	F(1)=F(3)-E1	100100
	F(2)=F(4)-1.0D0	100200
3	CONTINUE	100300
	CM=F(1)+C(1)*F(3)+C(2)*F(2)	100400
	DM=F(2)+C(1)*F(4)+C(2)*F(3)	100500
	DE=(VM-CM)/DM	100600
	ERROR=DE	100700
	AB=DABS(DE)	100800
	IF(AB-1.0D0)10,10,11	100900
11	DE=DE/AB	101000
10	E2=E1+DE	101100
	IF((E2+E1).EQ. 0.0D0) GO TO 4	101200
	IF(DABS((E2-E1)/(E2+E1))-3.0D-8)4,4,5	101300
5	CONTINUE	101400
	IF(N-NMAX)6,7,7	101500
7	CONTINUE	101600
	GO TO 4	101700

6 CONTINUE
N=N+1
E1=E2
GO TO (8,9),K
4 CONTINUE
RETURN
END

101800
101900
102000
102100
102200
102300
102400

	SUBROUTINE HARMON(R1,V1,ACC,TIME)	102500
	IMPLICIT REAL*8 (A-H,O-Z,S)	102600
	DIMENSION DATEEC(3,3),DATECT(3,3)	102700
	DIMENSION R1(3,8),V1(3,8),RR(3),ACC(3),TFMP(3),DATE(3,3),	102800
1	SDATE(3,3),DATET(3,3),SDATET(3,3),ADATE(3,3),ADATET(3,3)	102900
	DIMENSION A(3,3),EN(3,3),EMN(3,3),AR(3,3),LCT(8),ICT(9),	103000
1	CNM(36),SNM(36),ECN(3),PVA(9),CTT(8),CTR(8),UMT(45),VMT(45),	103100
2	LCTM(5),ICTM(6),CNMM(15),SNMM(15),CTTM(5),CTRM(5),UMTM(21),	103200
3	VMTM(21)	103300
	COMMON/ROT/ DATE,SDATE,DATET,SDATET,ADATE,ADATET,DATEEC,DATECT,EN	103400
	COMMON/XLIB/ SG,TA,XMLIB	103500
	COMMON C(1000),IC(50),Z(3),VV(3),NOR	103600
	COMMON/TUP/ TLU	103700
	DATA LCT/8,7,6,5,4,3,2,1/, LCTM/5,4,3,2,1/	103800
	EQUIVALENCE (C(200),CNM(1)), (C(236),SNM(1)),(C(272),CNMM(1))	103900
	EQUIVALENCE (C(287),SNMM(1))	104000
	KEY=1	104100
	IF(DABS(TLU-TIME) .LT. C(901)) GO TO 100	104200
	TLU=TIME	104300
	KEY=2	104400
	CALL ROTEQ(TIME,A)	104500
	CALL NUTAIT(TIME,OM,CR,DT,EN,EPSIL)	104600
	CALL MULT(EN,A,DATE)	104700
	DO 101 I=1,3	104800
	DU 101 J=1,3	104900
101	DATET(J,I) = DATE(I,J)	105000
100	CONTINUE	105100
	GO TO (20,4,80,80,5), NOR	105200
20	CONTINUE	105300
	NTE=8	105400
	ECN(1) = C(21)	105500
	ECN(2) = C(1)	105600
	ITIME = TIME	105700
	T2 = (TIME-ITIME)*86400.000	105800
	T1 = ITIME	105900
	DA = EN(2,1)	106000
	CALL GHA(T2,T1,GHAN,DA,OMEGA)	106100
	ECN(3) = GHAN*.0174532925200	106200
	CALL M1(R1(1,1),DATE,RR)	106300
	DO 1 I=1,3	106400
1	PVA(I) = RR(I)	106500
	CALL GETACC(LCT,ICT,CNM,SNM,ECN,PVA,CTT,CTB,UMT,VMT,NTE)	106600
	CALL M1 (PVA(7),DATET,ACC)	106700
	RETURN	106800
4	CONTINUE	106900
	GO TO (200,202), KEY	107000
202	CALL MNA(TIME,OM,CR,DT,EPSIL,RO,G,GP,WW,EMN)	107100
	CALL MULT(EMN,DATE,SDATE)	107200
	DO 201 I=1,3	107300
	DO 201 J=1,3	107400
201	SDATET(J,I) = SDATE(I,J)	107500
200	CONTINUE	107600
	DP=TIME	107700
	TP=DP/36525.00	107800
	T2P=TP*TP	107900
	T3P=T2P*TP	108000
	OM=12.1127900-.05295392200*DP +.002079500*TP	108100
1	+.00208100*T2P+.20-5*T3P	108200
	CR=64.37545200 +13.17639700*DP -.00113157500*TP	108300
1	-.0011301500*T2P+ .190-5*T3P	108400
	EPSIL=23.445758700-.0130940400*TP -.880-6*T2P +.50-6*T3P	108500
	OM=OM*(75)	108600
	CR=CR*(75)	108700
	EPSIL=EPSIL*(75)	108800
	XMLIB = 180.00*.0174532925200 + CR-OM+TA-SG	108900
	NTE=5	109000

	ECN(1) = C(22)	109100
	ECN(2) = C(2)	109200
	ECN(3) = 0.00	109300
	CALL M1(R1(1,2),SDATE,RR)	109400
	DO 2 I=1,3	109500
2	PVA(I) = RR(I)	109600
	CALL GETACC(LCTM,ICTM,CNMM,SNMM,ECN,PVA,CTTM,CTBM,IIMTM,VMTM,NTE)	109700
	CALL M1(PVA(7),SDATET,ACC)	109800
	RETURN	109900
5	CONTINUE	110000
	XJ2 = C(725)	110100
	XJ3 = C(726)	110200
	RE = C(25)	110300
	U = C(5)	110400
	R = FNORM(R1(1,5))	110500
	GO TO (300,302), KEY	110600
302	ITIME = TIME	110700
	T2 = TIME-ITIME	110800
	T1 = ITIME	110900
	CALL DATOUT (T1,T2,DATE,FDATE,U)	111000
	CALL ARES(DATE,FDATE,AR)	111100
	CALL MULT(AR,A,ADATE)	111200
	DO 301 I=1,3	111300
	DO 301 J=1,3	111400
301	ADATET(J,I) = ADATE(I,J)	111500
300	CONTINUE	111600
	CALL M1(R1(1,5),ADATE,RR)	111700
	R2 = R**2	111800
	R5 = R**5	111900
	R7 = R5*R2	112000
	RE2 = RE*RE	112100
	RE3 = RE2*RE	112200
	Z2 = RR(3)*RR(3)	112300
	Z3 = Z2*RR(3)	112400
	COEF = -1.5DO*U*XJ2*RE2/R5	112500
	DO 10 I=1,3	112600
10	PVA(I+6) = COEF*(-5.DO*Z2*RR(I)/R2 + RR(I))	112700
	PVA(9) = PVA(9) + COEF*2.DO*RR(3)	112800
	IF(XJ3.EQ.0.DO) GO TO 13	112900
	COEF = -.5DO*U*XJ3*RE3/R7	113000
	DO 14 I=1,3	113100
14	TEMP(I) = COEF*(-35.DO*Z3*RR(I)/R2 + 15.DO*RR(I)*RR(3))	113200
	TEMP(3) = TEMP(3) + COEF*(15.DO*Z2-3.DO*R2)	113300
	DO 15 I=1,3	113400
15	PVA(I+6) = PVA(I+6) + TEMP(I)	113500
13	CALL M1(PVA(7),ADATET,ACC)	113600
C	CONTINUE	113700
80	RETURN	113800
	END	113900

```

SUBROUTINE INTR1(TW,TF,NB,POS,INDM,VFL,DUM2) 114000
IMPLICIT REAL*8 (A-H,O-Z) 114100
C***** 114200
C      THIS VERSION OF THE 360 JPL DOUBLE PRECISION EPHEMERIS 114300
C      WAS MODIFIED BY JERRY S. LINNEKIN OF CODE 551 GSFC,GREENBELT MD, 114400
C      IT HAS BEEN MODIFIED TO HANDLE SEVEN BODIES INSTEAD OF THE 114500
C      NORMAL ELEVEN. THE BODIES AND ORDER ARE EARTH,MOON,SUN,VENUS,MARS, 114600
C      SATURN AND JUPITER. SATURN AND JUPITER HAVE BEEN INTERCHANGED 114700
C      TO CORRESPOND TO THE QUICK LOOK MISSION ANALYSIS PROGRAM. 114800
C      THE READ ROUTINE-GETTAP HAS BEEN MODIFIED TO USE THE DIRECT ACCESS 114900
C      READ FEATURE OF 360 FORTRANH. IN ADDITION,THE NUTATION VARIABLES 115000
C      HAVE BEEN ELIMINATED FROM THIS VERSION SO THAT AN EPHEMERIS 115100
C      RECORD WILL FIT ON ONE TRACK OF A 2316 DISK PACK. 115200
C      THE DECK AS IT APPEARS HERE IS SET UP AS A DIRECT REPLACEMENT 115300
C      FOR THE SINGLE PRECISION INTR1 IN THE QUICK LOOK MISSION 115400
C      ANALYSIS PROGRAM. 115500
C***** 115600
C      IN ADDITION TO THE ABOVE CHANGES,THE FOLLOWING COMMENT CARDS 115700
C      DESCRIBE THE CHANGES NECESSARY TO USE THIS PACKAGE WITH THE 115800
C      MARK2 PROGRAM ,THE MARK2 COVERAGE PROGRAM AND THE QUICK LOOK 115900
C      COVERAGE PROGRAM 116000
C      ***** MARK2 PROGRAM ***** 116100
C      SUBROUTINE ANTR (TW,TF,NB,POS,VEL) MK2 PROGRAM 116200
C      DATA NCENT/3,11,10,2,4,5,6/ MARK2 116300
C      NCENTR=NCENT(NB) FOR MARK 11 116400
C      ***** MARK2 COVERAGE PROGRAM***** 116500
C      SUBROUTINE ANTR1(TW,TF,NB,POS,VEL,DIS) MK2 COVERAGE PROGRAM 116600
C      DATA NCENT/3,11,10,2,4,5,6/ MARK2 116700
C      NCENTR=NCENT(NB) 116800
C      ***** COVER -QUICK LOOK COVERAGE PRNG ***** 116900
C      NO CHANGE NECESSARY DUE TO CAREFUL PLANNING BY PROGRAMMER 117000
C***** 117100
C      TO EXTEND THE EPHEMERIS FOR ALL BODIES,CHANGE THE FOLLOWING 117200
C      POS(21) TO POS(33),VEL(21) TO VEL(33) AND NCENT(7) TO NCENT(11) 117300
C      REPLACE THE NCENT DATA CARD WITH 117400
C      DATA NCENT/3,11,10,2,4,5,6,1,7,8,9/ 117500
C      THIS WILL RESULT IN THE FOLLOWING BODIES IN THE ORDER 117600
C      THAT THEY ARE LISTED EARTH,MOON,SUN,VENUS,MARS,JUPITER,SATURN, 117700
C      MERCURY,URANUS,NEPTUNE AND PLUTO. 117800
C***** 117900
C      ARGUMENT DESCRIPTION 118000
C      TW INPUT, WHOLE DAYS FROM 1950, REAL*8 118100
C      TF INPUT, FRACTIONAL DAYS FROM 1950, REAL*8 118200
C      NB INPUT, CENTRAL BODY NUMBER (1-EARTH, 2-MOON, 3-SUN, 118300
C      4-VENUS, 5-MARS, 6-SATURN, 7-JUPITER), INTEGER*4 118400
C      POS OUTPUT, POSITION ARRAY, POS(1)-POS(3), EARTH X,Y,Z 118500
C      VEL OUTPUT, VELOCITY ARRAY, REAL*8 118600
C      NCENTR CENTRAL BODY NUMBER (3-EARTH,11-MOON, 10-SUN, 2-VENUS, 118700
C      AU ASTRONOMICAL UNIT 118800
C      REM EQUATORIAL RADIUS OF EARTH 118900
C      4-MARS, 6-SATURN, 5-JUPITER) 119000
C      EMRAT EARTH MOON MASS RATIO 119100
C      REAL*8 JED,NUT 119200
C      REAL*8 JEDPRV 119300
C      REAL*8 JDN 119400
C      REAL*8 JEZ 119500
C      REAL*8 JDI 119600
C      DIMENSION POS(21),VEL(21),NCENT(7),IREQ(13),TABOUT(6,12),NUT(4) 119700
C      COMMON /CETBL1/ AU,REM,TPD,EMRAT 119800
C      COMMON /CETBL2/ ICW,NCENTR,IREQ 119900
C      COMMON /CETBL4/ TABOUT,NUT 120000
C      DATA NCENT/3,11,10,2,4,6,5/ 120100
C      DATA JEDPRV/0.00/,IERR/0/ 120200
C      DATA IFIRST/0/ 120300
C      DATA NCENTP/0/ 120400
C      IF(IFIRST.NE.0)GO TO 20 120500
C      ICW=1 120600

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IFIRST=1	120700
AU=149597900.D0	120800
REM=6378.1492D0	120900
TPD=86400.D0	121000
EMRAT=81.301D0	121100
20 DO 10 I=1,13	121200
10 IREQ(I)=2	121300
IF(TF-.5D0)38,39,39	121400
38 SEC1=TF*86400.D0	121500
GO TO 40	121600
39 DT=TW+.5D0	121700
SEC1=(TF-.5D0)*86400.D0	121800
GO TO 41	121900
40 DT=TW	122000
41 JD1=DT+2433282.5D0	122100
C*****	122200
C*****	122300
TSEC=SEC1	122400
JED=JD1	122500
JEZ=JED+TSEC	122600
NCENTR=NCENT(NB+1)	122700
IF(JEZ.EQ.JEDPRV.AND.NCENTR.EQ.NCENTP) GO TO 1	122800
JEDPRV=JEZ	122900
NCENTP=NCENTR	123000
CALL READE(JED,TSEC,IERR)	123100
IF(IERR.EQ.0) GO TO 1	123200
WRITE(6,100) IERR,NCENTR,ICW,JD3	123300
100 FORMAT(23HOF PHEMERIS ERROR, IERR=,I3,2I5,D14.2)	123400
1 CONTINUE	123500
DO 2 J=1,7	123600
DO 2 I=1,3	123700
II=(J-1)*3+I	123800
JJ=NCENT(J)	123900
POS(II)=TABOUT(I,JJ)	124000
2 VEL(II)=TABOUT(I+3,JJ)	124100
RETURN	124200
END	124300

SUBROUTINE ITER(IR,R1,V1,F,K,KK,DT,R,V)	124400
IMPLICIT REAL*8(A-H,O-Z,\$)	124500
COMMON C(1000),IC(50),Z(3),VV(3),NOR	124600
COMMON/STEPS/ STEP,XOLD	124700
DIMENSION X1(3),R1(3,8),R(3,8),V1(3,8),V(3,8),RR(3),VVV(3),CB(20)	124800
COUNT=0.DO	124900
ZRS=6.965D5	125000
XK=1	125100
F=0.DO	125200
DT=0.DO	125300
T=0.DO	125400
LK=1	125500
TOLD=0.DO	125600
FOLD=0.DO	125700
NN=1	125800
IF(KK.EQ.2) XK=-1	125900
C K=1 MEANS EARTH SHADOW, K=2 MEANS MOON SHADOW	126000
C K=3 MEANS OTHER PLANET SHADOW	126100
C KK=1 MEANS PENUMBRA, KK=2 MEANS UMBRA	126200
DO 2000 I=1,8	126300
DO 2000 J=1,3	126400
R(J,I)=R1	126500
2000 V(J,I)=V1	126600
GO TO (1,2,10),K	126700
1 DO 3 I=1,3	126800
3 X1(I)=R(I,1)-R(I,3)	126900
SEVA= ADOT(X1,R(I,1))	127000
RFS=FNORM(R(I,3))	127100
RFE= FNORM(R(I,1))	127200
DELS= DARSIN(6500.DO/RFE)*57.2957795D0	127300
ZRE=6500.DO	127400
GO TO 4	127500
2 DO 5 I=1,3	127600
5 X1(I)=R(I,2)-R(I,3)	127700
SEVA= ADOT(X1,R(I,2))	127800
RFS= FNORM(R(I,3))	127900
RFE= FNORM(R(I,2))	128000
DELS=DARSIN(1738.DO/RFE)*57.2957795D0	128100
ZRE=1738.DO	128200
GO TO 4	128300
10 DO 20 I = 1, 3	128400
20 X1(I) = R(I, NOR) - R(I,3)	128500
SEVA= ADOT(X1,R(I,NOR))	128600
RFS=FNORM(R(I,3))	128700
RFE= FNORM(R(I,NOR))	128800
DELS=DARSIN(C(NOR+20)/RFE)*57.2957795D0	128900
ZRE=C(NOR+20)	129000
4 CONTINUE	129100
ZRE=DSIGN(ZRE,XK)	129200
SIG=DARSIN((ZRS+ZRE)/RFS)*57.2957795D0	129300
F=SEVA+DELS*XK*SIG-180.DO	129400
IF(DABS(F).LE.0.000001D0) RETURN	129500
IF(COUNT.GT.100.DO) GO TO 11	129600
GO TO (6,7),LK	129700
6 LK=2	129800
DT=-STEP	129900
GO TO 8	130000
7 DT=(TOLD*F-T*FOLD)/(F-FOLD)	130100
8 FOLD=F	130200
TOLD=T	130300
T=DT	130400
CALL STEPD(NN,DT,TA,R1(1,1B),V1(1,1B),C(1B),RR,VVV,1,CB)	130500
TIM= C(593)+(XOLD+C(506)+T)/86400.DO	130600
CALL TFRAC(C(592),TIM,TT,TTF)	130700
CALL SHIFTP(1B,RR,VVV,TT,TTF,R,V)	130800
COUNT=COUNT+1.DO	130900

GO TO (1,2,10),K	131000
11 WRITE(6,12)	131100
12 FORMAT(1H0,22HMAX ITERATIONS IN ITER)	131200
STOP	131300
END	131400

SUBROUTINE KONSTK	131500
IMPLICIT REAL*8(A-H,O-Z,*)	131600
DIMENSION C(1000),IC(50)	131700
DIMENSION S(40,1),SSS(40,6)	131800
DIMENSION DNAME(2,6)	131900
DIMENSION D(7,3)	132000
C THE FOLLOWING STATEMENT(S) HAVE BEEN MANUFACTURED BY THE TRANSLATOR TO	132100
C COMPENSATE FOR THE FACT THAT EQUIVALENCE DOES NOT REORDER COMMON---	132200
COMMON C	132300
COMMON IC, SSS	132400
C DIMENSION C(1000),IC(50)	132500
C DIMENSION S(40,1),SSS(40,6)	132600
C DIMENSION DNAME(2,6)	132700
C DIMENSION D(7,3)	132800
C COMMON C, IC, SSS	132900
EQUIVALENCE (C(201),S(1,1)),(C(341),D(1,1)),(C(448),DNAME(1,1))	133000
C DEFINES CONSTANTS NEEDED BY PROGRAM	133100
C	133200
DO 1 I=1,1000	133300
1 C(I)=0.0D0	133400
C PLANETARY GRAVITATIONAL CONSTANTS (KM3/SEC2)	133500
C(1) = 398603.2D0	133600
C(2) = 4902.778D0	133700
C(3) = .13271545D12	133800
C(4) = 324767.5D0	133900
C(5)=42915.515D0	134000
C(6)=.12671059D9	134100
C(7)=10000.0D0	134200
C(8)=10000.0D0	134300
C RADIUS OF SPHERE OF INFLUENCE (KM)	134400
C(11)=925000.0D0	134500
C(12)=60000.0D0	134600
C(13)=1.0D10	134700
C(14)=616000.0D0	134800
C(15)=565000.0D0	134900
C(16)=.48D8	135000
C(17)=100000.0D0	135100
C(18)=100000.0D0	135200
C IMPACT RADIUS (KM)	135300
C(21)=6378.165D0	135400
C(22)=1738.0D0	135500
C(23)=694000.0D0	135600
C(24)=6050.0D0	135700
C(25) = 3417.0D0	135800
C(26)=71000.0D0	135900
C(27)=10000.0D0	136000
C(28)=10000.0D0	136100
C MINIMUM TIME STEP FOR OUTPUT (SEC)	136200
C(31)=43200.0D0	136300
C(32)=21600.0D0	136400
C(33)=1728000.0D0	136500
C(34)=43200.0D0	136600
C(35)=43200.0D0	136700
C(36)=86400.0D0	136800
C(37)=43200.0D0	136900
C(38)=43200.0D0	137000
C SIDEREAL ROTATION RATES (RAD/SEC)	137100
C(41)=.72921152D-4	137200
C INTERPOLATION INTERVALS FOR EPHEMERIS (DAYS)	137300
C(51)=40.0D0	137400
C(54)=40.0D0	137500
C(55)=40.0D0	137600
C(56)=100.0D0	137700
C NAMES OF EPHEMERIS BODIES	137800
DATA 0000HL/6H EARTH/	137900
C(61)=0000HL	138000

	DATA Q001HL/6H MOON/	138100
	C(62)=Q001HL	138200
	DATA Q002HL/6H SUN/	138300
	C(63)=Q002HL	138400
	DATA Q003HL/6H VENUS/	138500
	C(64)=Q003HL	138600
	DATA Q004HL/6H MARS/	138700
	C(65)=Q004HL	138800
	DATA Q005HL/6HJUPITER/	138900
	C(66)=Q005HL	139000
	DATA Q006HL/6HBODY 7/	139100
	C(67)=Q006HL	139200
	DATA Q007HL/6HBODY 8/	139300
	C(68)=Q007HL	139400
C	ASTRONOMICAL UNIT IN KM	139500
	C(70)=.149599	139600
C	SECONDS PER MEAN SOLAR DAY AND RECIPROCAL	139700
	C(71)=86400.000	139800
	C(72)=1.15740740-5	139900
C	SEMI-MAJOR AND SEMI-MINOR AXES OF THE EARTH (KM)	140000
	C(73)=6378.206400	140100
	C(74)=6356.583800	140200
C	DEGREE-RADIAN CONVERSIONS	140300
	C(75)=.01745329300	140400
	C(76) = 57.295779500	140500
	C(77) = 1.5707963200	140600
	C(78) = 3.1415926500	140700
	C(79) = 6.2831853000	140800
	DATA Q008HL/6H K/	140900
	C(85)=Q008HL	141000
	DATA Q009HL/6HM-KM/S/	141100
	C(86)=Q009HL	141200
	DATA Q010HL/6HEC-DEG/	141300
	C(87)=Q010HL	141400
	DATA Q011HL/6H U/	141500
	C(88)=Q011HL	141600
	DATA Q012HL/6HNITS A/	141700
	C(89)=Q012HL	141800
	DATA Q013HL/6HU--DEG/	141900
	C(90)=Q013HL	142000
	DATA Q014HL/6H FOU/	142100
	C(91)=Q014HL	142200
	DATA Q015HL/6HATOR D/	142300
	C(92)=Q015HL	142400
	DATA Q016HL/6HF DATE/	142500
	C(93)=Q016HL	142600
	DATA Q017HL/6H ECLI/	142700
	C(94)=Q017HL	142800
	DATA Q018HL/6HPTIC D/	142900
	C(95)=Q018HL	143000
	C(96)=Q016HL	143100
	DATA Q019HL/6H S/	143200
	C(97)=Q019HL	143300
	DATA Q020HL/6HELENDG/	143400
	C(98)=Q020HL	143500
	DATA Q021HL/6HGRAPHIC/	143600
	C(99)=Q021HL	143700
	C(122)=1.000	143800
C	**** THE FOLLOWING ARE EARTH POTENTIAL COEFFICIENTS ****	143900
C	C(200) THRU C(207) IS C(0,0) THRU C(7,0)	144000
C	C(208) THRU C(214) IS C(1,1) THRU C(7,1)	144100
C	C(215) THRU C(220) IS C(2,2) THRU C(7,2)	144200
C	C(221) THRU C(225) IS C(3,3) THRU C(7,3)	144300
C	C(226) THRU C(229) IS C(4,4) THRU C(7,4)	144400
C	C(230) THRU C(232) IS C(5,5) THRU C(7,5)	144500
C	C(233) THRU C(234) IS C(6,6) THRU C(7,6)	144600

C	C(235) IS C(7,7)	144700
C	C(236) THRU C(243) IS S(0,0) THRU S(7,0)	144800
C	C(244) THRU C(250) IS S(1,1) THRU S(7,1)	144900
C	C(251) THRU C(256) IS S(2,2) THRU S(7,2)	145000
C	C(257) THRU C(261) IS S(3,3) THRU S(7,3)	145100
C	C(262) THRU C(265) IS S(4,4) THRU S(7,4)	145200
C	C(266) THRU C(268) IS S(5,5) THRU S(7,5)	145300
C	C(269) THRU C(270) IS S(6,6) THRU S(7,6)	145400
C	C(271) IS S(7,7)	145500
	C(200)=0.000	145600
	C(201)=0.000	145700
	C(202)=-.108264500002D-2	145800
	C(203)=0.2545999999D-5	145900
	C(204) = .164 D-5	146000
	C(205) = .210 D-6	146100
	C(206) = -.645999999993D-6	146200
	C(207) = .332999999998D-6	146300
	C(208) = 0.00	146400
	C(209) = 0.00	146500
	C(210) = .209111899862 D-5	146600
	C(211) = -.542646846485 D-6	146700
	C(212) = -.676515582477D-7	146800
	C(213) = -.36979402246 D-7	146900
	C(214) = .14418923578 D-6	147000
	C(215) = .153563789676D-5	147100
	C(216) = .250708728736D-6	147200
	C(217) = .737902432577D-7	147300
	C(218) = .102117707526D-6	147400
	C(219) = .858383031385D-8	147500
	C(220) = .362552678174 D-7	147600
	C(221) = .782277124813D-7	147700
	C(222) = .508569773273D-7	147800
	C(223) = -.171778742888D-7	147900
	C(224) = -.11963004094D-8	148000
	C(225) = -.352147606138 D-8	148100
	C(226) = -.11198293875 D-8	148200
	C(227) = -.206336328204D-8	148300
	C(228) = -.166560812946D-9	148400
	C(229) = -.322776554575D-9	148500
	C(230) = .384108946188D-9	148600
	C(231) = -.252611520257 D-9	148700
	C(232) = .268980462153D-10	148800
	C(233) = -.931919036559D-11	148900
	C(234) = -.145066373826D-10	149000
	C(235) = .102027945339D-11	149100
	C(236) = 0.00	149200
	C(237) = 0.00	149300
	C(238) = 0.00	149400
	C(239) = 0.00	149500
	C(240) = 0.00	149600
	C(241) = 0.00	149700
	C(242) = 0.00	149800
	C(243) = 0.00	149900
	C(244) = 0.00	150000
	C(245) = 0.00	150100
	C(246) = .287312837632D-6	150200
	C(247) = -.444932466779D-6	150300
	C(248) = -.88203930746 D-7	150400
	C(249) = -.21243486397 D-7	150500
	C(250) = .114180308536 D-6	150600
	C(251) = -.872046750118 D-6	150700
	C(252) = -.183761983737 D-6	150800
	C(253) = .147804093315D-6	150900
	C(254) = -.375456547484D-7	151000
	C(255) = -.455316216648 D-7	151100
	C(256) = .162351886106 D-7	151200

C(257) = .225898207164 D-6	151300
C(258) = -.113546717887D-7	151400
C(259) = .231240615425 D-9	151500
C(260) = .642750579065D-9	151600
C(261) = .253546276422D-9	151700
C(262) = .485963696475D-8	151800
C(263) = .498321698304 D-9	151900
C(264) = -.196087502512D-8	152000
C(265) = -.216600056362D-9	152100
C(266) = -.145764420605D-8	152200
C(267) = -.369636026451D-9	152300
C(268) = .191117696793D-10	152400
C(269) = -.361118626660D-10	152500
C(270) = .437281413924D-11	152600
C(271) = .178085140954D-11	152700
C **** THE FOLLOWING ARE MOON POTENTIAL COEFFICIENTS ****	152800
C C(272) THRU C(276) IS C(0,0) THRU C(4,0)	152900
C C(277) THRU C(280) IS C(1,1) THRU C(4,1)	153000
C C(281) THRU C(283) IS C(2,2) THRU C(4,2)	153100
C C(284) THRU C(285) IS C(3,3) THRU C(4,3)	153200
C C(286) IS C(4,4)	153300
C C(287) THRU C(291) IS S(0,0) THRU S(4,0)	153400
C C(292) THRU C(295) IS S(1,1) THRU S(4,1)	153500
C C(296) THRU C(298) IS S(2,2) THRU S(4,2)	153600
C C(299) THRU C(300) IS S(3,3) THRU S(4,3)	153700
C C(301) IS S(4,4)	153800
C(272)=0.000	153900
C(273)=0.000	154000
C(274)=-.207108D-3	154100
C(275)=0.21D-4	154200
C(279)=0.34D-4	154300
C(281)=0.20716D-4	154400
C(284)=0.02583D-4	154500
C C(462)= FLAG FOR IMPACT	154600
C(462)=1.00	154700
C(506)=0.00	154800
C C(719)= REDUCTION FROM UNIVERSAL TO EPHM TIME 1966	154900
C(719)=40.000	155000
C C(720)= RECTIFICATION LIMIT IN ROUTINE DERIV	155100
C(720)=0.02500	155200
C C(725)= J2 OF MARS	155300
C(725)=0.1946667D-2	155400
C C(726)= J3 /F MARS	155500
C(726)=0.00	155600
C C(758) STANDS FOR TYPE OF INPUT	155700
C #1 EARTH MEAN EQUATOR AND EQUINOX OF 1950	155800
C #2 TRUE EQUINOX AND ECLIPTIC OF DATE	155900
C #3 SELENOGRAPHIC TRUE MOON EQUATOR OF DATE	156000
C #4 MARS MEAN EQUATOR OF DATE	156100
C #5 TRUE EARTH EQUATOR AND EQUINOX OF DATE	156200
C(758)=1.00	156300
C C(761) IS DAYS FOR INTEGRATION	156400
C(761)=180.000	156500
C(762)=1.000	156600
C(763)=0.000	156700
C(764)=86400.00	156800
C(765)=-1.000	156900
C(766)=1.000	157000
C(767)=5.000	157100
C(768)=111.00	157200
C---- C(769) SOLAR PRESS KEY 0.0=00 NOT INCLUDE 1.0= INCLUDE	157300
C(769)=0.000	157400
C---- C(770) AREA FOR SOLAR PRESSURES (CM.**2)	157500
C(770)=22225.00	157600
C---- C(771) MASS FOR SOLAR PRESS (GM.)	157700
C(771)=113000.00	157800

C----	C(772) REFLECTIVITY	157900
	C(772)=0.200	158000
C----	C(773) FRACTION OF PARTICLES REFLECTED	158100
	C(773)=1.000	158200
C----	C(774) SOLAR PRESS AT ONE A.U.	158300
	C(774)=4.7D-5	158400
C----	C(775) IS KEY FOR INPUT.=0. INPUT IS CARTESIAN.=1. INPUT IS	158500
C	ORBITAL ELEMENTS	158600
	C(775)=0.00	158700
C----	C(776) IS KEY FOR STOPPING AT APOGEE OR PERIGEE.	158800
C----	=0. DO NOT STOP, =1. STOP AT APOGEE, =-1. STOP AT PERIGEE	158900
	C(776)=0.00	159000
C----	C(777) IS THE KEY FOR EXTRA OUTPUT AND IS IN THE FORM ABCDEFGH.	159100
C----	0 MEANS DO NOT PRINT AND 1 MEANS PRINT.	159200
C----	A= CENTRAL BODY MEAN EARTH EQUATOR OF 1950	159300
C----	B= MOON FIXED	159400
C----	C= MARS MEAN EQUATOR OF DATE	159500
C----	G= CENTRAL BODY TRUE EARTH EQUATOR OF DATE	159900
C----	H=EARTH FIXED LATITUDE AND LONGITUDE	160000
	C(777)=10000011.	160100
C	C(901) IS DELTA T FOR UPDATING TRANSFORMATIONS IN HARMON	160200
	C(901)=15.00	160300
C	THESE CONSTANTS WERE DEFINED IN MAIN	160400
	IC(1)=0	160500
	IC(2)=0	160600
	RETURN	160700
	END	160800

	SUBROUTINE M1 (X,A,Y)	160900
	IMPLICIT REAL*8(A-H,O-Z,S)	161000
C	SUBROUTINE GIVES Y=AX	161100
	DIMENSION X(3),Y(3),A(3,3)	161200
C	DIMENSION X(3),Y(3),A(3,3)	161300
	DO 1 I=1,3	161400
	Y(I)=0.00	161500
	DO 1 J=1,3	161600
1	Y(I)=Y(I)+A(I,J)*X(J)	161700
	RETURN	161800
	END	161900

	SUBROUTINE MNA(TIME,OM,CR,DT,EPSIL,RN,G,GP,WW,FM)	162000
	IMPLICIT REAL*8(A-H,O-Z,\$)	162100
	DIMENSION EM(3,3),DF(3)	162200
	COMMON/XLIB/ SG,TA	162300
C		162400
C		162500
C		162600
	D = TIME	162700
	T = D/36525.D0	162800
	T2 = T*T	162900
	T3 = T2*T	163000
	A=13.064992D0	163100
	DO 6 I=1,3	163200
	DD=0.D0	163300
	DD=0	163400
	DD=DD*(A/360.D0)	163500
	DD=DD-IDINT(DD)	163600
	DF(I)=DD	163700
	GO TO (4,5,6),I	163800
4	A=.9856005D0	163900
	GO TO 6	164000
5	A=.1643586D0	164100
6	CONTINUE	164200
	G=215.54013D0+360.D0*DF(1)	164300
	GP=358.009067D0+360.D0*DF(2)	164400
	WW=196.745632D0+360.D0*DF(3)	164500
	G = G*.017453296D0	164600
	GP = GP*.017453296D0	164700
	WW = WW*.017453296D0	164800
	YN = 1.535D0*.017453296D0	164900
	RO = -.0297222D0*DCOS(G)+.0102777D0*DCOS(G+2.D0*WW)	165000
1	-.00305555D0*DCOS (2.D0*G+2.D0*WW)	165100
	TA = -.003333D0*DSIN(G)+.0163888D0*DSIN(GP)	165200
1	+.005D0*DSIN(2.D0*WW)	165300
	SG = -.0302777D0*DSIN(G) + .0102777D0*DSIN(G+2.D0*WW)	165400
1	-.00305555D0*DSIN (2.D0*G+2.D0*WW)	165500
	SG = (SG*.017453296D0)/DSIN (YN)	165600
	RO = RO*.017453296D0	165700
	TA = TA*.017453296D0	165800
	YN = YN + RO	165900
	RO = OM + SG + DT	166000
	CI = DCOS (RO)*DSIN (EPSIL)*DSIN (YN)	166100
1	+DCOS (EPSIL)*DCOS (YN)	166200
	SI = 1.D0 - CI**2	166300
	SI = DSQRT (SI)	166400
	SO = -DSIN (RO)*DSIN (YN)/SI	166500
	CO = 1.D0 - SO**2	166600
	CO = DSQRT (CO)	166700
	SD = -DSIN (RO)*DSIN (EPSIL)/SI	166800
	CD = -DSIN (RO)*SO*DCOS (EPSIL) - DCOS (RO)*CO	166900
	DL=ARKTNS(0,CD,SD)	167000
8	CONTINUE	167100
	CA = DL + (CR + TA) - (OM + SG)	167200
	SA = DSIN (CA)	167300
	CA = DCOS (CA)	167400
	RO = DCOS (RO)*DSIN (EPSIL)/(SI*CO)	167500
	EM(1,1) = CA*CO - SA*SO*CI	167600
	EM(1,2) = CA*SO + SA*CO*CI	167700
	EM(1,3) = SA*SI	167800
	EM(2,1) = -SA*CO - CA*SO*CI	167900
	EM(2,2) = -SA*SO + CA*CO*CI	168000
	EM(2,3) = CA*SI	168100
	EM(3,1) = SO*SI	168200
	EM(3,2) = -CO*SI	168300
	EM(3,3) = CI	168400
	RETURN	168500
	END	168600

	SUBROUTINE MULT(A,B,C)	168700
	IMPLICIT REAL*8(A-H,O-Z,\$)	168800
	DIMENSION A(3,3),B(3,3),C(3,3)	168900
C	DIMENSION A(3,3),B(3,3),C(3,3)	169000
	DO 1 I=1,3	169100
	DO 1 J=1,3	169200
	C(I,J) = 0.00	169300
	DO 1 K=1,3	169400
1	C(I,J) = C(I,J) + A(I,K)*B(K,J)	169500
	RETURN	169600
	END	169700

C

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SUBROUTINE NUTAIT (TIME,OM,CR,DT,EN,FPSIL)
IMPLICIT REAL*8(A-H,O-Z,$)
DIMENSION EN(3,3)
DIMENSION EN(3,3)
DD7=0.00
D = TIME
T = D/36525.000
T2 = T*T
T3 = T*T
OM= 12.11279000-.05295392200*O+.002079500*T+.0020810000*T2+.000002
20000*T3
CR = 64.37545200+13.17639700*O-.00113157500*T-.0011301500*T2+.0000
201900*T3
GP = 208.8439900+.1114040800*O-.0103340000*T-.0103430000*T2-.00001
220000*T3
VL = 280.0812100+.9856473400*O+.0003030000*(T+T2)
G = 282.0805300+.4706840-04*O+.0004552500*T+.0004575000*T2+.000003
200000*T3
OM = OM*.01745329600
CR = CR*.01745329600
GP = GP*.01745329600
VL = VL*.01745329600
G = G*.01745329600
DE1 = 25.58440000 * DCOS(OM)
DE2 = -.251100 * DCOS(2.00*OM)
DE3 = 1.533600*DCOS(2.00*VL)
DE4 = .066600* DCOS( 3.00* VL -G )
DE5 = -.025800 * DCOS( VL+G )
DE6 = -.018300 * DCOS( 2.00*VL-OM)
DE7 = -.006700 * DCOS( 2.00*GP - OM )
DE = DE1 + DE2 + DE3 + DE4 + DE5 + DE6 + DE7
DD1 = .245600 * DCOS(2.00*CR)
DD2 = .050800 * DCOS( 2.00* CR - OM)
DD3 = .036900 * DCOS(3.00* CR - GP )
DD4 = -.013900 * DCOS( CR+GP)
DD5 = -.008600 * DCOS( CR-GP+OM )
DD6 = .008300 * DCOS( CR-GP-OM )
DD8 = .006100 * DCOS( 3.00 * CR+GP - 2.00*VL )
DD9 = .006400 * DCOS( 3.00*CR -GP -OM)
DD = DD1 + DD2 + DD3 + DD4 + DD5 + DD6 + DD7 + DD8 + DD9
DT1 = -( 47.89270000 + .048200*T ) * DSIN(OM)
DT2 = .5800 * DSIN( 2.00*OM )
DT3 = -3.536100000 * DSIN( 2.00 * VL )
DT4 = -.137800 * DSIN( 3.00*VL -G )
DT5 = .059400 * DSIN( VL+G )
DT6 = .034400 * DSIN( 2.00*VL - OM)
DT7 = .012500 * DSIN( 2.00*GP - OM )
DT8 = .3500 * DSIN( VL-G )
DT9 = .012500 * DSIN( 2.00*VL - 2.00*GP )
DT = DT1 + DT2 + DT3 + DT4 + DT5 + DT6 + DT7 + DT8 + DT9
DS1 = -.565800 * DSIN( 2.00*CR )
DS2 = -.09500 * DSIN( 2.00*CR - OM )
DS3 = -.072500 * DSIN( 3.00*CR - GP )
DS4 = .031700 * DSIN( CR+GP )
DS5 = .016100 * DSIN( CR -GP +OM )
DS6 = .015800 * DSIN( CR -GP -OM )
DS7 = -.014400 * DSIN( 3.00*CR + GP - 2.00*VL )
DS8 = -.012200 * DSIN( 3.00*CR - GP - OM )
DS9 = .187500 * DSIN( CR - GP )
DS10 = .007800 * DSIN( 2.00*CR - 2.00*GP )
DS11 = .041400 * DSIN( CR + GP - 2.00*VL )
DS12 = .016700 * DSIN( 2.00*CR - 2.00*VL )
DS13 = -.008900 * DSIN( 4.00*CR - 2.00*VL )
DS = DS1+DS2+DS3+DS4+DS5+DS6+DS7+DS8+DS9+DS10+DS11+DS12+DS13
DE = .174532960-5*(DE+DD)
DT = .174532960-5*(DT+DS)

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EB = 23.4457587D0-.01309404D0*T-.00000088D0*T2+.0000005D0*T3	176400
EB = EB*.017453296D0	176500
EPSIL = EB+DE	176600
EN(1,1) = 1.0D0	176700
EN(1,2)=-DT*DCOS(EB)	176800
EN(1,3)=-DT*DSIN(EB)	176900
EN(2,1) = -EN(1,2)	177000
EN(2,2) = 1.0D0	177100
EN(2,3) = -DE	177200
EN(3,1) = -EN(1,3)	177300
EN(3,2) = DE	177400
EN(3,3) = 1.0D0	177500
RETURN	177600
END	177700

SUBROUTINE ORB(X,DX,U,NOUT)	177800
IMPLICIT REAL*8(A-H,O-Z,\$)	177900
DIMENSION C(1000)	178000
DIMENSION X(3),DX(3),B(3)	178100
C THE FOLLOWING STATEMENT(S) HAVE BEEN MANUFACTURED BY THE TRANSLATOR TO	178200
C COMPENSATE FOR THE FACT THAT EQUIVALENCE DOES NOT REORDER COMMON---	178300
COMMON C	178400
C COMMON C	178500
C DIMENSION C(1000)	178600
C DIMENSION X(3),DX(3),B(3)	178700
EQUIVALENCE (C(700),SMA),(C(701),FCC),(C(702),OINC),(C(703),OMG)	178800
1,(C(704),BEP),(C(705),RCA),(C(706),C3),(C(707),THET),(C(708),PERV)	178900
2,(C(709),P),(C(710),BB),(C(711),TPER)	179000
CALL CROSS(X,DX,B)	179100
R2 = DOT(X,X)	179200
R=DSQRT(R2)	179300
V2 = DOT(DX,DX)	179400
B2 = DOT(B,B)	179500
BB=DSQRT(B2)	179600
A=DOT(X,DX)/U	179700
P = B2/U	179800
C3 = V2-2.000*U/R	179900
SMA=-U/C3	180000
ECC=DSQRT(DABS(1.000+C3*P/U))	180100
OINC=ARKTNS(180,B(3),DSQRT(B(1)**2+B(2)**2))	180200
OMG= ARKTNS(360,-B(2),B(1))	180300
RCA=P/(1.000+ECC)	180400
THET=ARKTNS(360,(P-R),BB*A)	180500
BET= ARKTNS(360,X(2)*B(1)-X(1)*R(2),X(3)*BB)	180600
BEP= BET-THET	180700
IF(BEP) 2,3,3	180800
2 REP=BEP+6.283185300	180900
3 CONTINUE	181000
RTD=57.2957795100	181100
OINC=OINC*RTD	181200
OMG=OMG*RTD	181300
BEP=BEP*RTD	181400
PERV=DSQRT(DABS(C3+2.000*U/RCA))	181500
VIMP=PERV-DSQRT(U/RCA)	181600
CTAS=(P/R-1.000)/ECC	181700
IF(DABS(CTAS).LT.1.00) GO TO 200	181800
STAS=0.00	181900
CTAS=DSIGN(1.000,CTAS)	182000
GO TO 201	182100
200 STAS=DSQRT(1.000-CTAS*CTAS)	182200
STAS = DSIGN(STAS,A)	182300
201 CONTINUE	182400
THE=ARKTNS(180,CTAS,STAS)	182500
THET=THE*RTD	182600
CALL TCONIC(U,ECC,SMA,P,THE,TPER,FAC)	182700
TPER=TPER/86400.000	182800
IF(SMA)10,10,11	182900
10 WRITE (6,7)SMA,ECC,OINC,OMG,BEP,RCA,C3,THET,PERV, P,VIMP,TPER	183000
7 FORMAT(5H SMAD15.8,5H ECCD15.8,5H INCD15.8,5H LAND15.8,	183100
15H APFD15.8,5H RCAD15.8/5H C3D15.8,5H THETD15.8,5H PERVD15.8,	183200
25H SLRD15.8,5H IMPVD15.8,5H TPERD15.8)	183300
GO TO 12	183400
11 F1=A*U/DSQRT(U*SMA)	183500
F2=1.000-R/SMA	183600
SINE=F1/ECC	183700
COSE=F2/ECC	183800
E=ARKTNS(360,COSE,SINE)	183900
XMAN=(E-ECC*SINE)*RTD	184000
PERH = FAC * C(79) / 3600.00	184100
APBK=SMA*(1.00+ECC)	184200
WRITE (6,5)SMA,ECC,OINC,OMG,BEP,RCA,C3,THET,APBK, XMAN,PERH,T	184300

1PER	184400
5 FORMAT(5H SMAD15.8,5H ECCD15.8,5H INCD15.8,5H LAND15.8,	184500
15H APFD15.8,5H RCAD15.8/5H C3D15.8,5H THETD15.8,5H APOGD15.8,	184600
25H MAND15.8,5H PERHD15.8,5H TPERD15.8)	184700
12 CONTINUE	184800
RETURN	184900
END	185000

	SUBROUTINE ORB2X(X,VX,E,U)	185100
	IMPLICIT REAL*8(A-H,O-Z)	185200
	DIMENSION X(3),VX(3),EL(6),A(3,2)	185300
C	EL CONSISTS OF INPUT ORBITAL ELEMENTS	185400
C	(1) SEMI-MAJOR AXIS (+ IF ELLIPTIC, -FOR HYPERBOLIC)	185500
C	(2) ECCENTRICITY (LESS THAN 1. ELLIPTIC, GREATER HYPERBOLIC)	185600
C	(3) TRUE ANOMALY (DEGREES)	185700
C	***IF C379 CHANGED TO 1.; MEAN ANOMALY IS USED FOR INPUT	185800
	C379 = 0.00	185900
C	(4) LONGITUDE OF THE ASCENDING NODE (DEGREES)	186000
C	(5) INCLINATION (DEGREES)	186100
C	(6) ARGUMENT OF PERIAPSIS (DEGREES)	186200
	DATA DR/.01745329300/	186300
	COM=DCOS(DR*EL(4))	186400
	SOM=DSIN(DR*EL(4))	186500
	CIN=DCOS(DR*EL(5))	186600
	SNI=DSIN(DR*EL(5))	186700
	IF(C379)10,10,20	186800
20	XM=EL(3)*DR	186900
	ECC=EL(2)	187000
	E=XM+ECC*DSIN(XM)+(ECC**2/2.00)*DSIN(2.00*XM)+(ECC**3/24.00)*(9.	187100
	100*DSIN(3.00*XM)-3.00*DSIN(XM)+(ECC**4/192.00)*(64.00*DSIN(4.0	187200
	*0*XM)-32.00*DSIN(2.00*XM))	187300
	CTA=(DCOS(E)-ECC)/(1.00-ECC*DCOS(E))	187400
	STA=DSQRT(1.00-ECC**2)*DSIN(E)/(1.00-ECC*DCOS(E))	187500
	TAA=ARCTNS(180,CTA,STA)	187600
	GO TO 21	187700
10	CTA=DCOS(DR*EL(3))	187800
	STA=DSIN(DR*EL(3))	187900
	TAA=EL(3)*DR	188000
21	TBB=TAA+EL(6)*DR	188100
	CBA=DCOS(TBB)	188200
	SBA=DSIN(TBB)	188300
	A(1,1)=COM*CBA-(SOM*CIN)*SBA	188400
	A(2,1)=SOM*CBA+(COM*CIN)*SBA	188500
	A(3,1)=SNI*SBA	188600
	A(1,2)=-COM*SBA-(SOM*CIN)*CBA	188700
	A(2,2)=-SOM*SBA+(COM*CIN)*CBA	188800
	A(3,2)=SNI*CBA	188900
	P=EL(1)*(1.000-EL(2)**2)	189000
	R=P/(1.000+EL(2)*CTA)	189100
C	R IS THE RADIUS VECTOR MAGNITUDE	189200
	VR=EL(2)*STA*DSQRT(U/P)	189300
C	VR IS THE RADIAL COMPONENT OF VELOCITY	189400
	VT=DSQRT(U*(2.000/R-1.000/EL(1))-VR*VR)	189500
C	VT IS THE TANGENTIAL COMPONENT OF VELOCITY	189600
	DO 1 I=1,3	189700
	X(I)=R*A(I,1)	189800
	VX(I)=VR*A(I,1)+VT*A(I,2)	189900
1	CONTINUE	190000
	RETURN	190100
	END	190200

SUBROUTINE OUT(X,Y,D,ERROR,N,L,H)	190300
IMPLICIT REAL*8(A-H,O-Z,\$)	190400
DIMENSION A(3,3),EN(3,3),EMN(3,3),AR(3,3)	190500
DIMENSION DATE(3,3),SDATE(3,3),DATET(3,3),SDATET(3,3),ADATE(3,3),	190600
ADATET(3,3),DATEEC(3,3),DATECT(3,3),XX(3),XV(3)	190700
DIMENSION Y(20),D(20),ERROR(30)	190800
DIMENSION RATE(3),PERT(3),PERTT(3)	190900
DIMENSION DACC(3),CACC(3),UACC(3)	191000
DIMENSION R1(3,8),V1(3,8)	191100
DIMENSION XTEMP(3),VTEMP(3)	191200
DIMENSION DUM(3,3)	191300
COMMON/DISTRB/DACC,CACC,DACC	191400
COMMON /RNT/ DATE,SDATE,DATET,SDATET,ADATE,ADATET,DATEFC,DATECT	191500
COMMON/TIME/TW,TF	191600
COMMON C(1000),IC(50),Z(3),VV(3),NOR,INP	191700
COMMON/TUP/TLU	191800
COMMON/PRINT/ IC50,ISEL,MARDAT,ICENEC,IEAREC,ISUNEC,ICDATE,IEARFX	191900
DATA ST/-1./,ST1/-1./	192000
EQUIVALENCE (C(401),R1(1,1)),(C(425),V1(1,1))	192100
3 TIM =C(593)+(X+C(506))/86400.D0	192200
CALL TFRAC(C(592),TIM ,TW,TF)	192300
IF (C(122) .NE. 0.D0) GO TO 3000	192400
ST1 = TW	192500
ST = TF	192600
IF(C(594)-(C(506)+X).GT.0.D0) GO TO 50	192700
3000 IF(TW.EQ.ST1.AND.DABS(TF-ST).LE..0000200) GO TO 50	192800
DO 1002 JJ=1,3	192900
1002 PERT(JJ)=DACC(JJ)-CACC(JJ)	193000
ST1=TW	193100
ST=TF	193200
WRITE(6,9)	193300
9 FORMAT(1H0)	193400
CALL DATOUT(TW,TF,DAYM,FDATE,0)	193500
TP=TW+TF	193600
TLU=TP	193700
CALL ROTEQ(TP,A)	193800
CALL NUTAIT(TP,OM,CR,DT,EN,EPSIL)	193900
CALL MULT(EN,A,DATE)	194000
DUM(1,1)=1.D0	194100
DUM(1,2)=0.D0	194200
DUM(1,3)=0.D0	194300
DUM(2,1)=0.D0	194400
DUM(2,2)=DCOS(EPSIL)	194500
DUM(2,3)=DSIN(EPSIL)	194600
DUM(3,1)=0.D0	194700
DUM(3,2)=-DUM(2,3)	194800
DUM(3,3)= DUM(2,2)	194900
CALL MULT(DUM,DATE,DATEEC)	195000
DO 800 I=1,3	195100
DO 800 J=1,3	195200
800. DATET(J,I)=DATE(I,J)	195300
C	195400
100 IF(ICDATE.EQ.0) GO TO 30	195500
CALL M1(R1(1,NOR),DATE,XX)	195600
CALL M1(V1(1,NOR),DATE,XV)	195700
WRITE(6,48) C(NOR+60)	195800
48 FORMAT(1H0,A6,1X,'CENTERED',3X,'TRUE EARTH EQUATOR AND EQUINOX OF	195900
DATE')	196000
CALL OUTX(XX,XV,NOUT)	196100
CALL ORB(XX,XV,C(NOR),NOUT)	196200
30 IF(IC50.EQ.0.AND.C(777).NE.0.D0) GO TO 31	196300
WRITE(6,10) C(NOR+60)	196400
10 FORMAT(1H0,A6,1X,'HCENTERED',3X,'51HCENTRAL BODY MEAN EARTH EQUATOR	196500
AND EQUINOX OF 1950)	196600
CALL OUTX(R1(1,NOR),V1(1,NOR),NOUT)	196700
CALL ORB(R1(1,NOR),V1(1,NOR),C(NOR),NOUT)	196800

31	IF(IEARFX.EQ.0.OR.NOR.NE.1) GO TO 200	196700
	ITIME=TP	197000
	T2=(TP-ITIME)*86400.D0	197100
	T1=ITIME	197200
	DA=EN(2,1)	197300
	CALL GHA(T2,T1,GHAN,DA,OMEGA)	197400
	GHAN=GHAN*C(75)	197500
	CALL M1(R1(1,NOR),DATE,XTEMP)	197600
	SINT=DSIN(GHAN)	197700
	COST=DCOS(GHAN)	197800
	XX(1)= XTEMP(1)*COST+XTEMP(2)*SINT	197900
	XX(2)=-XTEMP(1)*SINT+XTEMP(2)*COST	198000
	XX(3)=XTEMP(3)	198100
	XLONGI=ARKTNS(180,XX(1),XX(2))*C(76)	198300
C		198400
200	CONTINUE	198500
	IF(ISEL.EQ.0.OR.NOR.NE.2) GO TO 300	198600
	CALL MNA(TP,OM,CR,DT,EPSIL,RO,G,GP,WW,EMN)	198700
	CALL MULT(EMN,DATE,SDATE)	198800
	DO 801 I=1,3	198900
	DO 801 J=1,3	199000
801	SDATE(J,I)=SDATE(I,J)	199100
	CALL M1(R1(1,NOR),SDATE,XX)	199200
	CALL M1(V1(1,NOR),SDATE,XV)	199300
	CALL M1(PERT,SDATE,PERTT)	199400
	WRITE(6,500) C(NOR+60)	199500
500	FORMAT(1H0,A6,1X,'FIXED TRUE MOON EQUATOR OF DATE')	199600
	CALL OUTX(XX,XV,NOUT)	199700
	CALL ORB(XX,XV,C(NOR),NOUT)	199800
300	CONTINUE	199900
	IF(MARDAT.EQ.0.OR.NOR.NE.5) GO TO 1001	200000
	CALL ARES(DAYM,FDATE,AR)	200100
	CALL MULT(AR,A,ADATE)	200200
	DO 802 I=1,3	200300
	DO 802 J=1,3	200400
802	ADATE(J,I)=ADATE(I,J)	200500
	CALL M1(R1(1,NOR),ADATE,XX)	200600
	CALL M1(V1(1,NOR),ADATE,XV)	200700
	CALL M1(PERT,ADATE,PERTT)	200800
	WRITE(6,700) C(NOR+60)	200900
700	FORMAT(1H0,A6,1X,35HCENTERED MARS MEAN EQUATOR OF DATE)	201000
600	CALL OUTX(XX,XV,NOUT)	201100
	CALL ORB(XX,XV,C(NOR),NOUT)	201200
C		201300
C		201400
1001	IOR=NOR	201500
400	CONTINUE	201600
	IF(IOR.EQ.3.AND.ISUNEC.EQ.0) GO TO 32	201900
	CALL M1(V1(1,IOR),DATEEC,XV)	202100
C		202200
	WRITE(6,900) C(IOR+60)	202300
900	FORMAT(1H0,A6,1X,'CENTERED TRUE ECLIPTIC AND EQUINOX OF DATE')	202400
	CALL OUTX(XX,XV,NOUT)	202500
C		202600
	IF(IOR.EQ.NOR) CALL ORB(XX,XV,C(NOR),NOUT)	202700
32	CONTINUE	202800
	IF(IOR.EQ.3.AND.NOR.NE.3) GO TO 14	202900
	IF(IOR.EQ.1) GO TO 1000	203000
	IOR=1	203100
	GO TO 400	203200
1000	IF(IOR.EQ.3) GO TO 14	203300
	IF(NOR.EQ.3) GO TO 14	203400
	IOR=3	203500
	GO TO 400	203600
14	CONTINUE	203700
	IF(NOR.NE.1.OR.IEARFX.EQ.0) GO TO 33	203800

	WRITE(6,3001) XLATI,XLONGI	203900
33	CONTINUE	204100
	WRITE(6,21)C(461)	204200
21	FORMAT(20HONUMBER OF STEPS IS D20.8)	204300
C		204400
C		204500
C		204600
50	RETURN	204700
	END	204800

	SUBROUTINE OUTX(X,VX,NOUT)	204900
	IMPLICIT REAL*8(A-H,O-Z,\$)	205000
	DIMENSION X(3),VX(3),C(6)	205100
C	DIMENSION X(3),VX(3),C(6)	205200
	CALL RVOUT(X,VX,C)	205300
	WRITE (6,5)X,VX,C	205400
	5 FORMAT(5H XD15.8,5H YD15.8,5H ZD15.8,5H DXD15.8,	205500
	1 5H DYD15.8,5H DZD15.8/5H RD15.8,5H DECD15.8,5H RAD15.8,	205600
	2 5H VD15.8,5H PTHD15.8,5H AZD15.8)	205700
	RETURN	205800
	END	205900

SUBROUTINE OVRLAY	206000
IMPLICIT REAL*8(A-H,O-Z,\$)	206100
COMMON S(1000),IC(5)	206200
DIMENSION BUFP(4),IND(4)	206300
16 FORMAT(4(I3,D12.8))	206400
994 FORMAT(1H0)	206500
995 FORMAT(4(5X,I3,D17.8))	206600
996 FORMAT('1',40X,13HOVERLAY INPUT)	206700
K=-1	206800
15 CONTINUE	206900
READ(5,16,END=20) (IND(I),BUFP(I),I=1,4)	207000
DO 10 N=1,4	207100
N=N	207200
GO TO (11,12,12,12),N	207300
11 CONTINUE	207400
IF(IND(N))13,13,17	207500
17 IF(K)18,19,19	207600
18 WRITE(6,996)	207700
K=0	207800
19 CONTINUE	207900
WRITE(6,995) (IND(J),BUFP(J),J=1,4)	208000
GO TO 14	208100
12 IF(IND(N)) 15,15,14	208200
14 CONTINUE	208300
J=IND(N)	208400
S(J)=BUFP(N)	208500
10 CONTINUE	208600
GO TO 15	208700
13 CONTINUE	208800
WRITE(6,994)	208900
RETURN	209000
20 STOP	209100
END	209200

	SUBROUTINE READE(JED,TSEC,IERR)	209300
	IMPLICIT REAL*8(A-H,O-Z)	209400
C	READE. READ,INTERPOLATE,TRANSLATE JPL EPHEMERIS	209500
C	J.E. EKELOUND, MESA SCIENTIFIC CORP., 1965 SEPT 15	209600
C	C.L. LAWSON, JPL, 1966 MAR 17	209700
C	READ JPL EPHEMERIS AT THE JULIAN EPHEMERIS DATE	209800
C	GIVEN BY (JED+TSEC/86400.DO)	209900
C		210000
C**	ITEMS COMMUNICATED THROUGH THE CALLING SEQUENCE **	210100
C		210200
C	JED REFERENCE JULIAN EPHEMERIS DATE.	210300
C	TSEC SECONDS OF EPHEMERIS TIME PAST JED.	210400
C	ANY COMBINATION OF VALUES OF JED AND TSEC	210500
C	IS ACCEPTABLE AS LONG AS (JED+TSEC/86400.DO)	210600
C	IS WITHIN THE RANGE OF THE EPHEMERIS TAPE	210700
C	BEING USED. HOWEVER TO OBTAIN THE	210800
C	FINEST POSSIBLE RESOLUTION IN INTERPOLATION	210900
C	THE NUMBER JED MUST BE AN EXACT MACHINE	211000
C	NUMBER. FOR EXAMPLE JED COULD BE A DATE ENDING	211100
C	WITH .0 OR .5 .	211200
C	IERR ERROR FLAG	211300
C	0=NO ERROR	211400
C	1=(JED+TSEC/86400.DO) LESS THAN FIRST DATE	211500
C	ON TAPE	211600
C	2=(JED+TSEC/86400.DO) GREATER THAN LAST DATE	211700
C	ON TAPE	211800
C	3=SOME IREQ(I) IS NOT 0,1, OR 2	211900
C	4=ICENT IS NOT IN THE RANGE 1 THRU 11	212000
C	5=ICW IS NOT 1,2, OR 3	212100
C		212200
C**	THE FOLLOWING ITEMS ARE INPUT THROUGH COMMON **	212300
C *	COMMON BLOCK CETBL1 *	212400
C	AU A.U. EXPRESSED IN DESIRED OUTPUT UNITS	212500
C	RE EQUATORIAL RADIUS OF EARTH IN DESIRED OUTPUT UNITS	212600
C	RE IS USED TO SCALE THE LUNAR EPHEMERIS	212700
C	TPD DESIRED NUMBER OF TIME UNITS PER DAY	212800
C	COMMON/CETBL2/ICW,ICENT ,IREQ(13)	212900
C		213000
C *	COMMON BLOCK CETBL2 *	213100
C	ICW FLAG INDICATING STATUS OF COMMON BLOCKS REC2 AND CETBL3	213200
C	1 MEANS NEITHER BLOCKS CONTAIN VALID DATA	213300
C	2 MEANS BOTH BLOCKS CONTAIN VALID DATA	213400
C	3 MEANS REC2 IS VALID, CETBL3 IS NOT	213500
C	USER MUST SET ICW=1 BEFORE INITIAL CALL	213600
C	ICENTR SPECIFIES CENTRAL BODY FOR COORDINATE	213700
C	TRANSLATION AS FOLLOWS..	213800
C	1 MERC 5 JUP 9 PLUTO	213900
C	2 VENUS 6 SAT 10 SUN	214000
C	3 EARTH 7 URANUS 11 MOON	214100
C	4 MARS 8 NEP	214200
C	IREQ(I) IREQ(I) SPECIFIES OUTPUT DESIRED FOR	214300
C	BODY NO. J.	214400
C	IREQ(J)=0 NO OUTPUT	214500
C	1 POSITION	214600
C	2 POSITION AND VELOCITY	214700
C	J RUNS FROM 1 TO 11 AS FOLLOWS..	214800
C	1 MERC 5 JUP 9 PLUTO	214900
C	2 VENUS 6 SAT 10 SUN	215000
C	3 EARTH 7 URANUS 11 MOON	215100
C	4 MARS 8 NEP 12 EARTH-MN-BARYCENTER	215200
C	13 NUTATION	215300
C *	COMMON BLOCK CETBL3 *	215400
C	TAB3 829 DOUBLE PREC. WORD BUFFER TO ACCOMMODATE J.D. AND EPHEMERIS.	215500
C	NUTAT 204 SINGLE PREC. WORD BUFFER TO ACCOMMODATE NUTATION DATA.	215600
C	CKSUM 1 S.P. WORD FOR CHECKSUM.	215700
C**	THE FOLLOWING ITEMS ARE OUTPUT THROUGH COMMON **	215800

C	* COMMON BLOCK CETRL4 *	215900
C	TABOUT(,) PLANETARY AND LUNAR OUTPUT, SCALED AND	216000
C	TRANSLATED WITH RESPECT TO CENTER.	216100
C	TABOUT (I,J) CONTAINS OUTPUT FOR	216200
C	BODY NO. J. (1 .LE. J .LE. 12)	216300
C	THE INDEX I IDENTIFIES COMPONENTS AS FOLLOWS..	216400
C	1=X 2=Y 3=Z	216500
C	4=XDOT 5=YDOT 6=ZDOT	216600
C	NUT() NOTATION OUTPUT	216700
C	NUT(1)=DELTA LONGITUDE	216800
C	NUT(2)=DELTA OBLIQUITY	216900
C	NUT(3)=TIME DERIVATIVE OF NUT(1)	217000
C	NUT(4)=TIME DERIVATIVE OF NUT(2)	217100
C		217200
C	COMMON /CETBL5/ BIVECT(6,13)	217300
C		217400
C	* COMMON BLOCK CETRL5 *	217500
C	BIVECT(,) WORKING ARRAY. CONTENTS ARE INTERPOLATED	217600
C	AND SCALED BUT NOT TRANSLATED. 1ST INDEX RUNS	217700
C	OVER X,Y,Z,XDOT,YDOT,ZDOT AS IN TABOUT	217800
C	BUT 2ND INDEX IS DIFFERENT AS FOLLOWS..	217900
C	BODIES 1 THRU 9 ARE HELIOCENTRIC.	218000
C	1 MERC 5 JUP 9 PLUTO	218100
C	2 VENUS 6 SAT 10 MOON REL TO EARTH	218200
C	3 ERTHMN 7 URANUS 11 ERTHMN REL TO EARTH	218300
C	4 MARS 8 NEP 12 ERTHMN REL TO MOON	218400
C	13 SEE 4092+	218500
C		218600
C	THE COMMON BLOCK 'CETBL9' IS FOR COMMUNICATION	218700
C	BETWEEN RDEP2 AND GETR2.	218800
C	COMMON /CETBL1/ AU,RE,TPD,EMRAT	218900
C	COMMON /CETBL3/ TAB3(829),NUTAT(204),CKSUM	219000
C	COMMON/CETBL4/TABOUT(6,12),NUT(4)	219100
C	COMMON/CETBL9/JD1,TDAY,JDIF,IERR1	219200
C	LOGICAL WFLAG	219300
C	INTEGER KREQ(12),MCENT(11),M1(20),JREQ(11), IPOS(11),IVEL(11)	219400
C	REAL NUTAT ,STP(11)	219500
C	DOUBLE PRECISION AU,RE,EMRAT, TPD,TAB3,BIVECT,TABOUT,NUT	219600
C	DOUBLE PRECISION JD1,TDAY,JDIF ,JED	219700
C	DOUBLE PRECISION TSEC,RAT, FAC,U(2,3),C,TFMP	219800
C	FAC=1/86400	219900
C	DATA FAC/1.1574074074074074D-5/	220000
C		220100
C	DATA STP/ 2.,8*4.,2*.5/	220200
C	DATA KREQ/5,5,2,6*5,4,3,1/	220300
C	DATA MCENT/15,15,0,6*15,10,5/	220400
C	DATA M1/11,0,10,11,0,12,10,0,12,0,3,3,3,0,0,3,13,13,0,0/	220500
C	DATA	220600
C	* IPOS /02,092,146,200,254,308,362,416,470,524,1/	220700
C	* IVEL /47,119,173,227,281,335,389,443,497,677,103/	220800
C	DATA U/6*0.00/	220900
C		221000
C	499 CONTINUE	221100
C	JD1=JED	221200
C	TDAY=TSEC*FAC	221300
C		221400
C	IERR1=IERR	221500
C	CALL GETTAP	221600
C		221700
C	IF(IERR1 .NE. 0) GO TO 5000	221800
C	IF(ICENT .GE. 1 .AND. ICENT .LE. 11) GO TO 10	221900
C	IERR1=4	222000
C	GO TO 5000	222100
C	10 CONTINUE	222200
C		222300
C	SET JREQ() TO CONTROL INTERPOLATION	222400

DO 20 I=1,10	222500
IF(IREQ(I) .GE. 0 .AND. IREQ(I) .LE. 2) GO TO 20	222600
IERR1=3	222700
GO TO 5000	222800
20 JREQ(I)=IREQ(I)	222900
C BARYCENTER FLAG	223000
JREQ(3)=IREQ(12)	223100
MAXPL=JREQ(1)	223200
DO 24 I=2,10	223300
24 MAXPL=MAX0(MAXPL,JREQ(I))	223400
MAXEM=MAX0(IREQ(3),IREQ(11))	223500
MAXALL=MAX0(MAXPL,MAXEM)	223600
IF(ICENT.EQ.3.OR.ICENT.EQ.11) GO TO 28	223700
C CENTER IS NOT EARTH OR MOON	223800
C 10=MOON,3=ERTHMN	223900
JREQ(10)=MAXEM	224000
JREQ(3)=MAX0(JREQ(3),MAXEM)	224100
JREQ(ICENT)=MAXALL	224200
GO TO 32	224300
C	224400
C CENTER IS EARTH OR MOON	224500
C 10=MOON,3=ERTHMN	224600
28 JREQ(10)=MAXALL	224700
JREQ(3)=MAXPL	224800
32 JREQ(11)=IREQ(13)	224900
LUNAR=JREQ(10)	225000
IBARY=JREQ(3)*3	225100
C	225200
C JREQ() IS NOW SET	225300
C	225400
SAVE=0.	225500
6001 CONTINUE	225600
DO 240 IBODY=1,11	225700
IF(JREQ(IBODY)) 240,240,40	225800
40 IF(STP(IBODY).EQ.SAVE) GO TO 165	225900
SAVE=STP(IBODY)	226000
160 TEMP=JDIF/SAVE	226100
KK=TEMP	226200
U(1,1)=TEMP-FLOAT(KK)	226300
IF(U(1,1))161,165,161	226400
161 CONTINUE	226500
U(2,1)=1.00-U(1,1)	226600
DO 163 IU=1,2	226700
U(IU,3)=U(IU,1)*U(IU,1)	226800
U(IU,2)=(U(IU,3)-1.00)/6.00	226900
163 U(IU,3)=(U(IU,3)-4.00)/20.00	227000
165 IF(IBODY-10) 169,167,220	227100
167 C=RE	227200
GO TO 172	227300
169 C=AU	227400
C INTERPOLATE IBODY=1,2,...,10	227500
172 IGET1=IPOS(IBODY)+KK*9	227600
IC1=1	227700
200 CONTINUE	227800
IF(U(1,1))203,201,203	227900
203 IGET2=IGET1+6	228000
DO 204 IGET=IGET1,IGET2,3	228100
BIVECT(IC1,IBODY)=	228200
* C*(U(2,1)*(TAB3(IGET)+)	228300
* U(2,2)*(TAB3(IGET+ 1)+	228400
* U(2,3)* TAB3(IGET+ 2)))+	228500
* U(1,1)*(TAB3(IGET+ 9)+	228600
* U(1,2)*(TAB3(IGET+10)+	228700
* U(1,3)* TAB3(IGET+11)))	228800
204 IC1=IC1+1	228900
GO TO 205	229000

201	IC2=IC1+2	229100
	DO 232 I=IC1,IC2	229200
	BIVECT(I,IBODY)=C*TAB3(IGET1)	229300
202	IGET1=IGET1+3	229400
205	CONTINUE	229500
	JREQ(1BODY)=JREQ(1BODY)-1	229600
	IF(JREQ(1BODY)) 240,240,207	229700
207	IGET1=IVEL(1BODY)+KK*9	229800
	IC1=4	229900
	C=C/TPD	230000
	GO TO 200	230100
C		230200
C	INTERPOLATE 1BODY=11 NUTATION	230300
C		230400
220	C=1.00	230500
	IGET1=IP0S(1BODY)+KK*6	230600
	IC1=1	230700
222	IGET2=IGET1+3	230800
225	IF(U(1,1))228,226,228	230900
228	DO 230 IGET=IGET1,IGET2,3	231000
	NUT(IC1)=	231100
	* C*(U(2,1)*(NUTAT(IGET)+	231200
	* U(2,2)*(NUTAT(IGET+1)+	231300
	* U(2,3)* NUTAT(IGET+2)))+	231400
	* U(1,1)*(NUTAT(IGET+6)+	231500
	* U(1,2)*(NUTAT(IGET+7)+	231600
	* U(1,3)* NUTAT(IGET+8))))	231700
230	IC1=IC1+1	231800
	GO TO 232	231900
226	DO 227 IGET=IGET1,IGET2,3	232000
	NUT(IC1)=C*NUTAT(IGET)	232100
227	IC1=IC1+1	232200
232	CONTINUE	232300
	JREQ(1BODY)=JREQ(1BODY)-1	232400
	IF(JREQ(1BODY)) 240,240,236	232500
236	C=C/TPD	232600
	IGET1=IVEL(1BODY)+KK*6	232700
	IC1=3	232800
	GO TO 222	232900
240	CONTINUE	233000
C		233100
C	INTERPOLATION IS FINISHED	233200
C	RESULTS ARE IN BIVECT(,)AND NUT()	233300
C	TEST MOON REQUEST	233400
	IF(LUNAR) 4020,4020,4010	233500
C	NOTE..EMRAT=EARTH MASS/MOON MASS	233600
C	SET BIVECT(,11)=ERTHMN CENTERED AT EARTH	233700
C	SET BIVECT' ,12)=ERTHMN CENTERED AT MOON	233800
4010	RAT=1.00/(EMRAT+1.00)	233900
	IMAX=LUNAR * 3	234000
	DO 4016 I=1,IMAX	234100
	BIVECT(I,11)=RAT*BIVECT(I,10)	234200
4016	BIVECT(I,12)=-EMRAT*BIVECT(I,11)	234300
C		234400
4020	WFLAG=.FALSE.	234500
	KCENT=MCENT(ICENT)	234600
C		234700
C	BEGIN TRANSLATION LOOP	234800
C		234900
	DO 4108 1BODY=1,12	235000
	IF(IREQ(1BODY)) 4108,4108,4024	235100
4024	IMAX=IREQ(1BODY)*3	235200
	KASE=KCENY+KREQ(1BODY)	235300
	K1=M1(KASE)	235400
	GO TO (4032,4040,4032,4048,4052,	235500
	* 4032,4068,4040,4048,4056,	235600

* 4032,4076,4076,4040,4028,	235700
* 4084,4088,4088,4064,4080),KASF	235800
C	235900
C KASE=15	236000
4028 K1=IBODY	236100
C KASE=1,3,6,11	236200
4032 DO 4036 I=1,IMAX	236300
4036 TABOUT(I,IBODY)=BIVECT(I,K1)	236400
GO TO 4108	236500
C KASE=2,8,14	236600
4040 DO 4044 I=1,IMAX	236700
4044 TABOUT(I,IBODY)=0.00	236800
GO TO 4108	236900
C KASE=4,9	237000
4048 K2=3	237100
GO TO 4100	237200
C KASE=5	237300
4052 L2=11	237400
GO TO 4060	237500
C KASE=10	237600
4056 L2=12	237700
4060 K1=IBODY	237800
K2=13	237900
GO TO 4092	238000
C KASE=19	238100
4064 K1=ICENT	238200
C KASE=7	238300
4068 DO 4072 I=1,IMAX	238400
4072 TABOUT(I,IBODY)=-BIVECT(I,K1)	238500
GO TO 4108	238600
C KASE=12,13	238700
4076 K2=KASE-1	238800
GO TO 4100	238900
C KASE=20	239000
4080 K1=IBODY	239100
C KASE=16	239200
4084 K2=ICENT	239300
GO TO 4100	239400
C KASE=17,18	239500
4088 L2=ICENT	239600
K2=KASE-6	239700
4092 IF(WFLAG) GO TO 4100	239800
WFLAG=,TRUE.	239900
C	240000
C BIVECT(,13) IS AN AUXILIARY VECTOR	240100
C NEEDED WHEN KASE=5,10,17,18.	240200
C FOR KASE=05 BIVECT(,13)=EARTH CENTERED AT SUN	240300
C FOR KASE=10 BIVECT(,13)=MOON CENTERED AT SUN	240400
C FOR KASE=17,18 BIVECT(,13)=ERTHMN CENTERED AT ICENT	240500
C	240600
DO 4096 I=1,IBARY	240700
4096 BIVECT(I,13)=BIVECT(I,3)-BIVECT(I,L2)	240800
4100 DO 4104 I=1,IMAX	240900
4104 TABOUT(I,IBODY)=BIVECT(I,K1)-BIVECT(I,K2)	241000
4108 CONTINUE	241100
5000 IERR=IERR1	241200
RETURN	241300
END	241400

SUBROUTINE ROTEQ(TIME,A)	241500
IMPLICIT REAL*8(A-H,O-Z,\$)	241600
DIMENSION A(3,3)	241700
T = TIME/36525.D0	241800
T2 = T*T	241900
T3 = T2*T	242000
A(1,1) = 1.D0 - .00029697D0*T2 - .0000001300*T3	242100
A(1,2) = -.02234988D0*T - .00000676D0*T2 + .00000221D0*T3	242200
A(2,1) = -A(1,2)	242300
A(1,3) = -.00971711D0*T + .00000207D0*T2 + .00000096D0*T3	242400
A(3,1) = -A(1,3)	242500
A(2,2) = 1.D0 - .00024976D0*T2 - .0000001500*T3	242600
A(2,3) = -.00010859D0*T2 - .00000003D0*T3	242700
A(3,2) = A(2,3)	242800
A(3,3) = 1.D0 - .00004721D0*T2 + .00000002D0*T3	242900
RETURN	243000
END	243100

	SUBROUTINE RVOUT(A,B,C)	243200
	IMPLICIT REAL*8(A-H,O-Z,\$)	243300
	DIMENSION A(3),B(3),C(6)	243400
C	C IS RADIUS, LAT, LON, VELOCITY, GAMMA, AZIMUTH	243500
	CALL SPER(A,C)	243600
	C(4)=FNORM(B)	243700
	C(5)=90.00-ADOT(A,B)	243800
	VE=B(2)*A(1)-B(1)*A(2)	243900
	VN=C(1)*B(3)-A(3)*DOT(A,B)/C(1)	244000
	C(6)=57.2957795100*ARKTNS(180,VN,VE)	244100
	RETURN	244200
	END	244300

SUBROUTINE SHADOW(R1,V1,X, STEP)	244400
IMPLICIT REAL*8(A-H,O-Z,S).	244500
COMMON C(1000),IC(50),Z(3),VV(3),NOR	244600
COMMON /SHAD/SHADK	244700
DIMENSION R1(3,8),V1(3,8)	244800
DIMENSION X1(3)	244900
DIMENSION R(3,8),V(3,8)	245000
DATA IPFLAG/1/,IUFLAG/1/,IMFLAG/1/,IMUFLAG/1/, FLAG/0./,FLAG1/0./,	245100
1FLAG2/0./,FLAG3/0./	245200
DATA IVFLAG/1/,IVUFLAG/1/,PFLAG/0./,PUFLAG/0./	245300
6 FORMAT(1H0,15HBODY CENTER IS ,A6)	245400
IF(STEP.EQ.0.00)RETURN	245500
GO TO (41,41,505 ,400,400,400),NOR	245600
41 CONTINUE	245700
DO 4 I=1,3	245800
4 X1(I)=R1(I,1)-R1(I,3)	245900
SEVA=ADOT(X1,R1(1,1))	246000
RFS=FNORM(R1(1,3))	246100
RFE=FNORM(R1(1,1))	246200
DELS=DARSIN(6500.00/RFE)*57.295779500	246300
IF(SEVA-90.00) 300,300,301	246400
301 ZRS=6.965D5	246500
ZRE=6500.00	246600
ZPSIG=DARSIN((ZRS+ZRE)/RFS)*57.295779500	246700
FS=SEVA+DELS+ZPSIG-180.00	246800
IF(FS) 300,302,302	246900
302 FLAG=1.00	247000
IF(IPFLAG.NE.1) GO TO 1000	247100
K=1	247200
N=1	247300
IPFLAG=2	247400
KK=1	247500
WRITE(6,5)	247600
5 FORMAT(1H0,60HPROBE ENTERED EARTH PENUMBRA. TIME AND ORBIT ARE GIV	247700
1EN BELOW)	247800
SHADK=1.000	247900
GO TO 20	248000
1000 CONTINUE	248100
ZSIGMA=DARSIN((ZRS-ZRE)/RFS)*57.295779500	248200
FS=DELS-ZSIGMA+SEVA-180.00	248300
IF(FS)303,304,304	248400
304 FLAG1=1.00	248500
IF(IUFLAG.NE.1) GO TO 310	248600
K=1	248700
IUFLAG=2	248800
N=2	248900
KK=2	249000
WRITE(6,7)	249100
7 FORMAT(1H0,57HPROBE ENTERED EARTH UMBRA. TIME AND ORBIT ARE GIVEN	249200
18 BELOW)	249300
SHADK=1.000	249400
GO TO 20	249500
300 FLAG=0.00	249600
303 FLAG1=0.00	249700
310 DO 30 I=1,3	249800
30 X1(I)=R1(I,2)-R1(I,3)	249900
SEVA=ADOT(X1,R1(1,2))	250000
IF(SEVA-90.00) 2000,2000,901	250100
901 ZRS=6.965D5	250200
ZRE=1738.00	250300
ZPSIG=DARSIN((ZRS+ZRE)/RFS)*57.295779500	250400
DELM=DARSIN(C(22)/FNORM(R1(1,2)))*57.295779500	250500
FS=SEVA+DELM+ZPSIG-180.00	250600
IF(FS) 2000,902,902	250700
902 FLAG2=1.00	250800
IF(IMFLAG.NE.1) GO TO 3000	250900

K=2	251000
IMFLAG=2	251100
N=3	251200
KK=1	251300
WRITE(6,8)	251400
8 FORMAT(1H0,59HPROBE ENTERED MOON PENUMBRA. TIME AND ORBIT ARE GIVE	251500
1N BELOW)	251600
SHADK=1.000	251700
GO TO 20	251800
3000 CONTINUE	251900
ZSIGMA=DARSIN((ZRS-ZRE)/RFS)*57.295779500	252000
FS=DELM-ZSIGMA+SEVA-180.00	252100
IF(FS)2001,904,904	252200
904 FLAG3=1.00	252300
IF(IMUFLG.NE.1) GO TO 2010	252400
K=2	252500
IMUFLG=2	252600
N=4	252700
KK=2	252800
WRITE(6,9)	252900
9 FORMAT(1H0,56HPROBE ENTERED MOON UMBRA. TIME AND ORBIT ARE GIVEN B	253000
1ELOW)	253100
SHADK=1.000	253200
GO TO 20	253300
2000 FLAG2=0.00	253400
2001 FLAG3=0.00	253500
2010 CONTINUE	253600
IF(IPFLAG.NE.2.OR.FLAG.NE.0.00) GO TO 11	253700
WRITE(6,12)	253800
12 FORMAT(1H0,61HPROBE HAS LEFT EARTH PENUMBRA. TIME AND ORBIT ARE GI	253900
1VEN BELOW)	254000
SHADK=0.000	254100
K=1	254200
N=5	254300
KK=1	254400
IPFLAG=1	254500
GO TO 20	254600
11 IF(IUFLAG.NE.2.OR.FLAG1.NE.0.00) GO TO 14	254700
WRITE(6,1)	254800
13 FORMAT(1H0,58HPROBE HAS LEFT EARTH UMBRA. TIME AND ORBIT ARE GIVEN	254900
1 BELOW)	255000
SHADK=0.000	255100
KK=2	255200
N=6	255300
K=1	255400
IUFLAG=1	255500
GO TO 20	255600
14 IF(IMFLAG.NE.2.OR.FLAG2.NE.0.00) GO TO 15	255700
WRITE(6,16)	255800
16 FORMAT(1H0,60HPROBE HAS LEFT MOON PENUMBRA. TIME AND ORBIT ARE GIV	255900
1EN BELOW)	256000
SHADK=0.000	256100
KK=1	256200
K=2	256300
N=7	256400
IMFLAG=1	256500
GO TO 20	256600
15 IF(IMUFLG.NE.2.OR.FLAG3.NE.0.00) GO TO 505	256700
WRITE(6,18)	256800
18 FORMAT(1H0,57HPROBE HAS LEFT MOON UMBRA. TIME AND ORBIT ARE GIVEN	256900
1BELOW)	257000
SHADK=0.000	257100
K=2	257200
N=8	257300
KK=2	257400
IMUFLG=1	257500

C
C
C

20	CALL ITER(NOR,R1,V1,FS,K,KK,DT,R,V)	257600
	TIM=C(593)+(X+C(506)+DT)/86400.DO	257700
	CALL TFRAC(C(592),TIM,TT,TTF)	257800
	CALL DATOUT(TT,TTF,DATE,FDATE,0)	257900
		258000
		258100
		258200
	GO TO (1000,310,3000,2010,11,14,15,505 ,405,502,503,505),N	258300
400	DO 401 I=1,3	258400
401	X1(I)=R1(I,NOR)-R1(I,3)	258500
	SEVA=ADOT(X1,R1(1,NOR))	258600
	RFS=FNORM(R1(1,3))	258700
	RFE=FNORM(R1(1,NOR))	258800
	DELS=DARSIN(C(NOR+20)/RFE)*57.295779500	258900
	IF(SEVA-90.DO)500,500,402	259000
402	ZRS=6.96505	259100
	ZRE=C(NOR+20)	259200
	ZPSIG=DARSIN((ZRS+ZRE)/RFS)*57.295779500	259300
	FS=SEVA+DELS+ZPSIG-180.DO	259400
	IF(FS)500,403,403	259500
403	PFLAG=1.DO	259600
	IF(IVFLAG.NE.1) GO TO 405	259700
	K=3	259800
	N=9	259900
	IVFLAG=2	260000
	KK=1	260100
	WRITE(6,404)C(NOR+60)	260200
404	FORMAT(1H0,26HPROBE ENTERED PENUMBRA OF ,A6,30HTIME AND ORBIT ARE	260300
	1GIVEN BELOW)	260400
	SHADK=1.000	260500
	GO TO 20	260600
405	CONTINUE	260700
	ZSIGMA=DARSIN((ZRS-ZRE)/RFS)*57.295779500	260800
	FS=DELS-ZSIGMA+SEVA-180.DO	260900
	IF(FS)501,406,406	261000
406	PUFLAG=1.DO	261100
	IF(IVUFLG.NE.1) GO TO 502	261200
	K=3	261300
	IVUFLG=2	261400
	N=10	261500
	KK=2	261600
	WRITE(6,407) C(NOR+60)	261700
407	FORMAT(1H0,23HPROBE ENTERED UMBRA OF ,A6,30HTIME AND ORBIT ARE GIV	261800
	1EN BELOW)	261900
	SHADK=1.000	262000
	GO TO 20	262100
500	PFLAG=0.DO	262200
501	PUFLAG=0.DO	262300
502	IF(IVFLAG.NE.2.OR.PFLAG.NE.0.DO) GO TO 503	262400
	WRITE(6,504) C(NOR+60)	262500
504	FORMAT(1H0,27HPROBE HAS LEFT PENUMBRA OF ,A6,30HTIME AND ORBIT ARE	262600
	1 GIVEN BELOW)	262700
	SHADK=0.000	262800
	K=3	262900
	N=11	263000
	KK=1	263100
	IVFLAG=1	263200
	GO TO 20	263300
503	IF(IVUFLG.NE.2.OR.PUFLAG.NE.0.DO) GO TO 505	263400
	WRITE(6,506) C(NOR+60)	263500
506	FORMAT(1H0,24HPROBE HAS LEFT UMBRA OF ,A6,30HTIME AND ORBIT ARE GI	263600
	1VEN BELOW)	263700
	SHADK=0.000	263800
	KK=2	263900
	N=12	264000
	K=3	264100

IVUFLG=1
GO TO 20
505 CONTINUE
RETURN
END

264200
264300
264400
264500
264600

SUBROUTINE SHIFTP(NOR,R,V,TW,TF,RR,VV)	264700
IMPLICIT REAL*(A-H,O-Z,\$)	264800
DIMENSION C(1000),IC(50),R(3),V(3),RR(3,8),VV(3,8),PO(22),VE(22),	264900
1R1(3,2),V1(3,2),N(2),SPAR(20,2),T1(2,2)	265000
DIMENSION X(3),W(3)	265100
COMMON C , IC	265200
EQUIVALENCE (C(663),R1(1,1)),(C(681),V1(1,1)),(C(695),T1(1,1)),	265300
1(IC(1),IB1), (IC(2),IB2), (IC(12),N(1)), (C(71),SPMSD), (C(3),US)	265400
2,(C(801),PO(1)), (C(823),VE(1)), (C(561),SPAR(1,1))	265500
3,(C(699),SWNET)	265600
IC(2)=0.DO	265700
IF(SWNET)100,100,18	265800
100 DIS=1.D10	265900
DO 1 I=1,3	266000
X(I)=R(I)	266100
1 W(I)=V(I)	266200
NM1=NOR-1	266300
IF(NOR-6)4,3,2	266400
2 KKK=-1	266500
NM1=2	266600
GO TO 7	266700
3 NM1 = 6	266800
4 CONTINUE	266900
KKK=0	267000
IF(IB1-6)5,5,6	267100
5 IF(IB2-6)9,9,6	267200
6 KKK=1	267300
7 CONTINUE	267400
DO 8 I=1,2	267500
K=I+6	267600
TT=(IDINT(TW-T1(1,I))+TF-T1(2,I))*SPMSD	267700
CALL STEPD(N(I),TT,TA,R1(1,1),V1(1,1),US,RR(1,K),VV(1,K),1,	267800
1SPAR(1,I))	267900
8 CONTINUE	268000
9 CONTINUE	268100
CALL INTR1(TW,TF,NM1,PO,1,VE,DIS)	268200
IF(KKK)10,12,12	268300
10 NOR=NOR	268400
DO 11 I=1,3	268500
X(I)=X(I)+RR(I,NOR)	268600
11 W(I)=W(I)+VV(I,NOR)	268700
12 CONTINUE	268800
DO 13 J=1,5	268900
DO 13 I=1,3	269000
L=3*J-3+I	269100
RR(I,J)=X(I)-PO(L)	269200
13 VV(I,J)=W(I)-VE(L)	269300
DO 14 I=1,3	269400
RR(I,6)=X(I)-PO(I+18)	269500
14 VV(I,6)=W(I)-VE(I+18)	269600
IF(KKK)15,17,15	269700
15 DO 16 I=1,2	269800
K=I+6	269900
DO 16 J=1,3	270000
RR(J,K)=RR(J,3)-RR(J,K)	270100
16 VV(J,K)=VV(J,3)-VV(J,K)	270200
17 CONTINUE	270300
GO TO 35	270400
18 TT=((TW-T1(1,1))+TF-T1(2,1))*SPMSD	270500
M=2	270600
CALL STEPD(M,TT,TA,R1(1,1),V1(1,1),C(3),RR(1,1),VV(1,1),1,	270700
1SPAR(1,1))	270800
TT=((TW-T1(1,2))+TF-T1(2,2))*SPMSD	270900
IF(IC(1)+IC(2)-3)19,19,25	271000
19 M=2	271100
CALL STEPD(M,TT,TA,R1(1,2),V1(1,2),C(1),RR(1,2),VV(1,2),1,	271200

1 SPAR(1,2))	271300
DO 24 I=1,3	271400
IF(NOR-2)20,21,22	271500
20 RR(I,3)=-RR(I,1)	271600
VV(I,3)=-VV(I,1)	271700
RR(I,1)=0.00	271800
VV(I,1)=0.00	271900
GO TO 23	272000
21 RR(I,3)=-RR(I,1)-RR(I,2)	272100
VV(I,3)=-VV(I,1)-VV(I,2)	272200
RR(I,2)=0.00	272300
VV(I,2)=0.00	272400
GO TO 23	272500
22 RR(I,2)=RR(I,2)+RR(I,1)	272600
VV(I,2)=VV(I,2)+VV(I,1)	272700
RR(I,3)=0.00	272800
VV(I,3)=0.00	272900
23 DO 24 J=1,3	273000
RR(I,J)=R(I)-RR(I,J)	273100
VV(I,J)=V(I)-VV(I,J)	273200
24 CONTINUE	273300
GO TO 35	273400
25 M=2	273500
IF(IC(1)-3)27,27,26	273600
26 K=IC(1)	273700
GO TO 28	273800
27 K=IC(2)	273900
28 CONTINUE	274000
CALL STEPD(M,TT,TA,R1(1,2),V1(1,2),C(3),RR(1,K),VV(1,K),1,	274100
1 SPAR(1,2))	274200
DO 34 I=1,3	274300
IF(NOR-3)29,31,32	274400
29 RR(I,3)=-RR(I,1)	274500
VV(I,3)=-VV(I,1)	274600
IF(K.EQ.3) GO TO 30	274700
RR(I,K)=RR(I,K)-RR(I,1)	274800
VV(I,K)=VV(I,K)-VV(I,1)	274900
30 RR(I,1)=0.00	275000
VV(I,1)=0.00	275100
GO TO 33	275200
31 RR(I,3)=0.00	275300
VV(I,3)=0.00	275400
GO TO 33	275500
32 RR(I,1)=-RR(I,K)+RR(I,1)	275600
VV(I,1)=-VV(I,K)+VV(I,1)	275700
RR(I,3)=-RR(I,K)	275800
VV(I,3)=-VV(I,K)	275900
RR(I,K)=0.00	276000
VV(I,K)=0.00	276100
33 RR(I,1)=R(I)-RR(I,1)	276200
VV(I,1)=V(I)-VV(I,1)	276300
RR(I,3)=R(I)-RR(I,3)	276400
VV(I,3)=V(I)-VV(I,3)	276500
IF(K.EQ.1.OR.K.EQ.3) GO TO 34	276600
RR(I,K)=R(I)-RR(I,K)	276700
VV(I,K)=V(I)-VV(I,K)	276800
34 CONTINUE	276900
35 CONTINUE	277000
RETURN	277100
END	277200

	SUBROUTINE SOLAR (R, SACC)	277300
	IMPLICIT REAL * 8 (A-H, I-Z)	277400
	COMMON C(1000)	277500
	DIMENSION R(3), SACC(3), RX(3)	277600
	P=C(774)	277700
	A=C(770)	277800
	EM=C(771)	277900
	GAMMA=C(772)	278000
	SIGMA=C(773)	278100
	C1=P*A*(1.0 + 2.0/3.0*GAMMA + 1.0/3.0*GAMMA*SIGMA)/EM	278200
	DO 11 J=1,3	278300
	RX(J)=R(J) / 1.495D8	278400
11	C O N T I N U E	278500
	RAU=(RX(1)**2 + RX(2)** 2 +RX(3)**2)**0.5	278600
	C2=C1/RAU**3	278700
	DO 12 K=1,3	278800
	SACC(K)=C2*RX(K)*1.0D-5	278900
12	C O N T I N U E	279000
100	RETURN	279100
	END	279200

	SUBROUTINE SPER(X,Y)	279300
	IMPLICIT REAL*8(A-H,O-Z,S)	279400
C	CONVERTS CARTESIAN TO SPHERICAL. RETURNS IN DEG	279500
	DIMENSION X(3),Y(3)	279600
C	DIMENSION X(3),Y(3)	279700
	RTD=.572957795D+02	279800
	A=X(1)*X(1)+X(2)*X(2)	279900
	Y(1)=DSQRT(A+X(3)*X(3))	280000
	Y(2)=DATAN(X(3)/DSQRT(A))*RTD	280100
	Y(3)=ARKTNS(180, X(1),X(2))*RTD	280200
	RETURN	280300
	END	280400

	SUBROUTINE STEPD(N,T,TA,R,V,U,RR,VV,M,SR)	280500
	IMPLICIT REAL*8(A-H,O-Z,S).	280600
C	CB IS A STORAGE VECTOR WHOSE ELEMENTS ARE	280700
C	(1) INITIAL TRUE ANOMALY (11) ANGULAR MOMENTUM SQUARED H2	280800
C	(2) SEMI-LATUS RECTUM (12) ANGULAR MOMENTUM MAGNITUDE H	280900
C	(3) ECCENTRICITY (13) MU TIMES RADIUS MAGNITUDE UR	281000
C	(4) RADIUS-SQUARED (14) R DOT V	281100
C	(5) RADIUS MAGNITUDE (15) H2-UR	281200
C	(6) SEMI-MAJOR AXIS (A) (16) H*ROOTV	281300
C	(7) ABSOLUTE VALUE OF (A) (17) U/(R*H2)	281400
C	(8) MEAN MOTION (18) RV/H	281500
C	(9) TIME COEFFICIENT R/ABA (19) TIME FROM PERIAPSIS (+ OR -)	281600
C	(10) TIME COEFFICIENT RV/SQRT(UA) (20) SWITCH 1 ELLIP, 2 HYPER	281700
	DIMENSION R(3),V(3),HVEC(3),HR(3),VV(3),F(4),CH(20)	281800
	DIMENSION SB(20)	281900
C	DIMENSION R(3),V(3),HVEC(3),HR(3),VV(3),F(4),CH(20)	282000
C	DIMENSION SB(20)	282100
C		282200
C		282300
C		282400
C		282500
	N=N	282600
	GO TO (1,7),N	282700
1	CONTINUE	282800
	PI=.3141592650+01	282900
	TP1=.6283185300+01	283000
	CB(4)=DOT(R,R)	283100
	CB(5)=DSORT(CB(4))	283200
	V2=DOT(V,V)	283300
	CB(14)=DOT(R,V)	283400
	VM=DSORT(V2)	283500
	CB(6)=CB(5)/(2.000-CB(5)*V2/U)	283600
	CB(7)=DABS(CB(6))	283700
	CB(8)=DSORT(U/CB(7))/CB(7)	283800
	CB(9)=CB(5)/CB(7)	283900
	CB(10)=CB(14)/DSORT(U*CB(7))	284000
	CALL CROSS(R,V,HVEC)	284100
	CB(11)=DOT(HVEC,HVEC)	284200
	CB(12)=DSORT(CB(11))	284300
	CB(13)=U*CB(5)	284400
	CB(2)=CB(11)/U	284500
	EC2=1.000-CB(2)/CB(6)	284600
	IF(EC2.GE.(-1.0-6).AND.EC2.LE.0.00) GO TO 200	284700
	CB(3)=DSORT(EC2)	284800
	GO TO 201	284900
200	CB(3)=0.00	285000
201	CONTINUE	285100
	CB(15)=CB(11)-CB(13)	285200
	CB(16)=CB(12)*CB(14)	285300
	CB(17)=U/(CB(5)*CB(11))	285400
	CB(18)=CB(14)/CB(12)	285500
	CB(1)=ARKTNS(180,CB(15),CB(16))	285600
	TA2=CB(1)	285700
	IF(CB(6))3,3,2	285800
2	CONTINUE	285900
	CB(20)=1.000	286000
	E1=CB(8)*T	286100
	GO TO 4	286200
3	CONTINUE	286300
	CB(20)=2.000	286400
	E1=0.000	286500
4	CONTINUE	286600
	CALL TCONIC(U,CB(3),CB(6),CB(2),TA2,TFP,FAC)	286700
	N=N	286800
	GO TO (6,5),N	286900
5	CONTINUE	287000

	T=TFP-CB(19)+TAP*PD	287100
	GO TO 12	287200
6	CONTINUE	287300
	CH(19)=TFP	287400
	N=2	287500
	DO 60 I=1,20	287600
60	SB(I)=CB(I)	287700
	GO TO 700	287800
7	CONTINUE	287900
	DO 70 I=1,20	288000
70	CH(I)=SB(I)	288100
700	CONTINUE	288200
	PD=TPI/CB(8)	288300
	IF(M)8,8,11	288400
8	CONTINUE	288500
C	TA IS THE INCREMENTAL TRUE ANOMALY	288600
	CT=DCOS(TA)	288700
	ST=DSIN(TA)	288800
	EF=CT-ST*CB(18)	288900
	GE=ST*CB(4)/CB(12)	289000
	R2OR1=CB(11)/(CB(13)+CB(15)*CT-CB(16)*ST)	289100
	EF=R2OR1*EF	289200
	GE=R2OR1*GE	289300
	EFD=CB(17)*(CB(14)-CB(14)*CT-CB(12)*ST)	289400
	GED=(CB(15)+CB(13)*CT)/CB(11)	289500
	TA2=CB(1)+TA	289600
	TAP=IDINT(TA2/TPI)	289700
	TA2=TA2-TPI*TAP	289800
	IF(IDINT(TA2/PI)) 9,4,10	289900
9	TAP=TAP-1.000	290000
	GO TO 4	290100
10	TAP=TAP+1.000	290200
	GO TO 4	290300
11	CONTINUE	290400
	K=CB(20)	290500
	EMDT=CB(8)*T	290600
	CALL GOTOR(K,EMDT,CH(9),F,E1)	290700
	EF=-F(2)/CH(9)+1.000	290800
	GE=-F(1)/CB(8)+T	290900
	R0A=F(2)+CB(9)*F(4)+CB(10)*F(3)	291000
	EFD=-CB(7)*CB(8)*F(3)/(CB(5)*R0A)	291100
	GED=-F(2)/R0A+1.000	291200
	TA=ARKTNS(180,CB(4)*EF+CB(14)*GE,CB(12)*GE)	291300
	IF(K-1)110,110,12	291400
110	CONTINUE	291500
	TAP=IDINT(T/PI)	291600
	IF(TA+T)111,112,112	291700
111	TAP=TAP+DSIGN(1.000,T)	291800
112	TA=TA+TAP*PI	291900
12	CONTINUE	292000
	DO 13 I=1,3	292100
	RR(I)=EF*R(I)+GE*V(I)	292200
	VV(I)=EFD*R(I)+GED*V(I)	292300
13	CONTINUE	292400
	RETURN	292500
	END	292600

SUBROUTINE TCONIC(U,EC,A,SLR,TA2,T,FAC)	292700
IMPLICIT REAL*8(A-H,O-Z,S)	292800
TANG(Q000FL)=DSIN(Q000FL)/DCOS(Q000FL)	292900
AB = DABS(A)	293000
FAC=AB*DSORT(AB/U)	293100
ECA=(1.000-EC)/(1.000+EC)	293200
ABF = DSORT(DABS(FCA))	293300
THE=TANG(.500*TA2)	293400
IF(ABE-.0000500)11,11,12	293500
12 CONTINUE	293600
ECA=2.000*DATAN(ABE*THE)	293700
IF(A)14,11,13	293800
13 T=FAC*(ECA-FC*DSIN(ECA))	293900
GO TO 16	294000
14 ANG=.78539816300 + ECA/2.00	294100
T=FAC*(EC*TANG(ECA)-DLNG(TANG(ANG)))	294200
GO TO 16	294300
11 FAC=DSORT(SLR**3/11)*2.000/((1.000+EC)**2)	294400
EC1=ECA*THE**2	294500
T=FAC*(THE+THE**3*((1.000-2.000*FCA)/3.000-(2.000-3.000*ECA)*EC1/5	294600
1.000+(3.000-4.000*ECA)*EC1**2/7.000-(4.000-5.000*FCA)*EC1**3/9.000	294700
2))	294800
16 CONTINUE	294900
RETURN	295000
END	295100

SUBROUTINE TERM(X,Y,D,F)	295200
IMPLICIT REAL*8(A-H,O-Z,\$)	295300
COMMON C(1000),IC(50),Z(3),VV(3),NOR	295400
COMMON/APPER/ FPROLD ,OLD,XMAX	295500
DIMENSION R1(3,8),V1(3,8)	295600
DIMENSION Y(20),D(20)	295700
COMMON/STEPS/ STEP,XOLD	295800
EQUIVALENCE (C(401),R1(1,1)), (C(425),V1(1,1))	295900
DATA XOLD/0./	296000
STEP = X-XOLD	296100
XOLD=X	296200
XOLD=XOLD	296300
Y(7)=X+C(506)	296400
C(461) = C(461)+1.D0	296500
F=C(594)-(C(506)+X)	296600
IF(C(776).EQ.0.D0) GO TO 5	296700
FPR=C(776)*(90.D0-ADOT(R1(1,NOR),V1(1,NOR)))	296800
IF (FPR.GT. 0.D0 .AND. X .NE. 0.D0) OLD=FPR	296900
IF(FPROLD.EQ.0.D0.AND.FPR.GT.0.D0) GO TO 5	297000
IF (X .EQ. 0.D0 .OR. OLD .EQ. 0.D0) GO TO 5	297100
FPROLD=1.D0	297200
F=FPR	297300
5 CONTINUE	297400
IF(C(1000))4000,10,10	297500
10 IF(DABS(X+C(506)).LE.XMAX) GO TO 4000	297600
XMAX=DABS(X+C(506))	297700
IF(XMAX-C(1000)*86400.D0)4000,11,11	297800
11 CONTINUE	297900
CALL SHADOW(R1,V1,XOLD,STEP)	298000
4000 CONTINUE	298100
IF(FNORM(R1(1,NOR)).GT.C(NOR+20)) GO TO 2	298200
WRITE(6,3) C(NOR+60)	298300
3 FORMAT(1H0,19HPROBE HAS IMPACTED ,A6)	298400
F=0.D0	298500
C(122)=10.D0	298600
C(462)=0.D0	298700
RETURN	298800
2 CONTINUE	298900
IOR=3	299000
IF(FNORM(R1(1,1)).LT.C(11)) IOR=1	299100
IF(FNORM(R1(1,2)).LT.C(12)) IOR=2	299200
IF(FNORM(R1(1,4)).LT.C(14)) IOR=4	299300
IF(FNORM(R1(1,5)).LT.C(15)) IOR=5	299400
IF(FNORM(R1(1,6)).LT.C(16)) IOR=6	299500
IF(IOR.EQ.NOR) GO TO 1	299600
NOR=IOR	299700
F=0.D0	299800
C(122)=2.D0	299900
RETURN	300000
1 IF(C(122).EQ.0.D0.AND.F.GT.0.D0) F=0.D0	300100
RETURN	300200
END	300300

SUBROUTINE TFRAC(T1,T2,TW,TF)	300400
IMPLICIT REAL*8(A-H,O-Z,S).	300500
TW=T1	300600
TF=T2	300700
3 CONTINUE	300800
IF(TF)1,2,2	300900
1 CONTINUE	301000
TW=TW-1.0D0	301100
TF=TF+1.0D0	301200
GO TO 3	301300
2 CONTINUE	301400
TDUM=IDINT(TF)	301500
TW=TW+TDUM	301600
TF=TF-TDUM	301700
RETURN	301800
END	301900

	SUBROUTINE TIMEC(T1,T2,T3,T4)	302000
	IMPLICIT REAL*8(A-H,O-Z,\$)	302100
C	T1 IS AN INPUT IN FORM (YEARS FROM 1900)(MONTH OF YEAR)	302200
C	(DAY OF MONTH	302300
C	WRITTEN AS 6501.12 FOR JAN. 12, 1965	302400
C	T2 IS AN INPUT IN FORM (HOUR OF DAY)(MINUTE OF HOUR)	302500
C	(SECOND OF MINUTE)	302600
C	WRITTEN AS 1301.3032 FOR 1PM, 1 MINUTE, 30.32 SECOND	302700
C	T3 IS WHOLE DAYS FROM 1950 OUTPUT	302800
	T4=0.000	302900
	TA=IDINT(T1)	303000
	TA1=TA/100.000+.0100	303100
	TY1= IDINT(TA1)	303200
	TY= TY1-60.000	303300
	IY=TY	303400
	IF (IY) 15,15,16	303500
15	CONTINUE	303600
	WRITE (6,17)	303700
17	FORMAT (37H EXIT FROM TIMEC. DATE 1960 OR BEFORE)	303800
	CALL EXIT	303900
16	CONTINUE	304000
	ND=3652	304100
	K=1	304200
	DO 1 I=1, IY	304300
	KK=K-I	304400
	IF (KK) 2,2,3	304500
2	CONTINUE	304600
	ND=ND + 366	304700
	K=K+4	304800
	GO TO 1	304900
3	CONTINUE	305000
	ND=ND +365	305100
1	CONTINUE	305200
	TY2=TA-TY1*100.000+.100	305300
	IY2=IDINT(TY2)	305400
	IF (IY2) 10,10,11	305500
11	CONTINUE	305600
	IF (12-IY2) 10,12,12	305700
10	CONTINUE	305800
	WRITE (6,13)	305900
13	FORMAT(37H INPUT TIME IS WRONG. EXIT FROM TIMEC)	306000
	CALL EXIT	306100
12	CONTINUE	306200
	DO 4 I=1,IY2	306300
	I=I	306400
C	JAN FEB MAR APRIL MAY JUNE JULY AUG SEPT OCT NOV	306500
	GO TO (4,6,7,6,8,6,8,6,6,8,6,8),I	306600
6	CONTINUE	306700
	ND=ND + 31	306800
	GO TO 4	306900
7	CONTINUE	307000
	IF(KK-1)9,14,9	307100
14	CONTINUE	307200
	ND=ND +29	307300
	GO TO 4	307400
9	CONTINUE	307500
	ND=ND +28	307600
	GO TO 4	307700
8	CONTINUE	307800
	ND=ND +30	307900
4	CONTINUE	308000
	TB1=(T1-TA)*100.000+.100	308100
	ND=ND+IDINT(TB1)	308200
	ND=ND-1	308300
	T3=ND	308400
	TA=IDINT(T2)	308500

T4=(T2-TA)/864.000	308600
T8=TA/100.000+.100	308700
T81=IDINT(T8)	308800
T82=TA-T81*100.000+.100	308900
T83=IDINT(T82)	309000
T4=T4+T81/24.000+T83/24.000/60.000	309100
RETURN	309200
END	309300

SUBROUTINE TRAJ(T1D,T1F,R,V,NE)	309400
IMPLICIT REAL*8(A-H,O-Z,\$)	309500
COMMON C(1000),IC(50),Z(3),VV(3),NOR	309600
COMMON/TIME/TW,TF	309700
DIMENSION R1(3,8),V1(3,8),R(3),V(3),Y(20),D(20)	309800
EQUIVALENCE (C(401),R1(1,1)),(C(425),V1(1,1))	309900
J=2	310000
N=6	310100
L=0	310200
C(461)=0.00	310300
C(506)=0.00	310400
C(590)=T1D	310500
C(591)=T1F	310600
C(594)=(C(590)-C(592)+C(591)-C(593))*86400.00	310700
IF(C(594).EQ.0.00) RETURN	310800
Y(9)=-1.00	310900
M=C(763)	311000
G=DSIGN(120.00,C(594))	311100
Y(8)=C(764)	311200
2 DO 1 I=1,6	311300
1 Y(I)=0.00	311400
X=0.00	311500
CALL FNOL2(J,N,G,L,M,NE,X,Y,D,DERIV,TERM,OUT)	311600
IF(C(122).EQ.1.00) GO TO 3	311700
IF(C(122).EQ.2.00) GO TO 6	311800
IF(C(122).EQ.10.00) RETURN	311900
IF(C(594)-(C(506)+X).LE.0.00) GO TO 3	312000
4 CONTINUE	312100
C(506)=C(506)+X	312200
C(122)=1.00	312300
DO 5 I=1,3	312400
C(I+499)=R1(I,NOR)	312500
5 C(I+502)=V1(I,NOR)	312600
GO TO 2	312700
6 CONTINUE	312800
C(122)=1.00	312900
WRITE(6,7) C(NOR+60)	313000
7 FORMAT(20HOBODY CENTER IS NOW A6)	313100
DO 8 I=1,3	313200
C(I+499)=R1(I,NOR)	313300
8 C(I+502)=V1(I,NOR)	313400
C(506)=C(506)+X	313500
GO TO 2	313600
3 CONTINUE	313700
DO 13 I=1,3	313800
R(I)=R1(I,NOR)	313900
13 V(I)=V1(I,NOR)	314000
C(122)=1.00	314100
C(592)=TW	314200
C(593)=TF	314300
RETURN	314400
END	314500

APPENDIX B

EXAMPLES

CASE 1 Apoapsis Printout*

Case 1 is an example of the input and output formats for printout at apoapsis. A detailed explanation will be helpful.

INPUT

C array	Variable
750	Semimajor axis of 53500 km.
751	Eccentricity is .86915888
752	True anomaly is 180 deg.
753	Right ascension of node is 45 deg.
754	Inclination to reference plane is 30 deg.
755	Argument of periapsis is 45 deg.
756	Epoch date is March 13, 1971
757	Epoch time is 0 ^h 0 ^m 0 ^s
(758) [†]	Input reference coordinate system is Earth mean equator and equinox of 1950, January 1, 0 ^h
759	Stop date is March 17, 1971
760	Stop time is 0 ^h
761	Apoapsis printout is wanted; therefore c(761) is total integration time of 4 days.
(762) [†]	= 1. for apoapsis printout
763	Apoapsis printout is wanted.
764	Apoapsis printout is wanted.
(765) [†]	No shadow is wanted
(767) [†]	Built-in error control used.
(768) [†]	Include harmonics for Earth, Moon and Mars whichever is the central body.
(769) [†]	No solar pressure — ignore c(770) through c(774).
775	Input in keplerian elements.
776	Printout at apogee only.
777	Three types of output requested: (1) Central body; mean earth equator and equinox of 1950 (2) Central body; true ecliptic and equinox of date (3) Sun-centered; true ecliptic and equinox of date.

* Apoapsis printout is a form of exact print and requires restarting the integrator

† Built-in value is used; therefore not included in input

OUTPUT

The first block of output shows that shadow times have not been requested and that central body oblateness of the Earth, Moon or Mars, whichever is the central body, is requested. However in this case, no oblateness is calculated since Venus is the central body.

The next block of output is the epoch time and the input transformed into the mean Earth equator and equinox of 1950, January 1 at 0^h, which is the working coordinate system of TRIP.

Next comes the epoch input transformed to those output options specified. In this case, the initial position of the satellite was at apoapsis. This is followed by similar output at the requested times. The output definitions are as follows:

X → DZ	State vector in km and km/sec.
R	Radius magnitude (km)
DEC	Declination of satellite in degrees referenced to the stated coordinate plane
RA	Right ascension or longitude of the satellite in degrees referenced to the stated coordinate plane.
V	Velocity magnitude in km/sec.
PTH	Flight path angle in degrees
AZ	Azimuth in degrees
SMA	Semimajor axis in km
ECC	Eccentricity
INC	Inclination in degrees to the reference plane
LAN	Longitude of the ascending node in degrees
APF	Argument of perifocus in degrees
RCA	Radius of closest approach (periapsis) in km
C3	Twice the total energy per unit mass in km^2/sec^2 ($-\mu/a$)
THET	True anomaly in degrees
APOG	Apoapsis in km
MAN	Mean anomaly in degrees.
PERH	Period in hours
TPER	Time to periapsis in days.

In the final block is the number of integration steps taken. Since printout at apoapsis, periapsis or exact time steps requires restarting the numerical integrator, this is the number of steps taken from the previous output time.

OVERLAY INPUT

750 0.535000000 05	751 0.540154800 00	752 0.180000000 03	753 0.660000000 02
754 0.300000000 02	755 0.450000000 02	756 0.710313000 04	757 0.00
758 0.710317000 04	760 0.00	761 0.400000000 01	763 0.100000000 04
764 0.00	766 0.400000000 01	775 0.100000000 01	776 0.100000000 01
777 0.100101000 03	0 0.00	0 0.00	0 0.00

SHANNON IS NOT REQUESTED

HARMONICS OF EARTH IS INCLUDED

HARMONICS OF MOON IS INCLUDED

HARMONICS OF MARS IS INCLUDED

SOLAR RADIATION PRESSURE IS NOT INCLUDED

INPUT IN MEAN EO AND FO OF 1950

MARCH 13, 1971, 13HRS, 04MIN, 0.05SEC

JULIAN DATE 2441023.50000000

X=0.669871810 06 Y=0.933012690 05 Z=0.35353440 05 NX=0.608201270 00 NY=0.436673150 01 NZ=0.230370000 00

R=0.100000000 06 DEC=0.207048160 02 RA=0.941069980 02 V=0.651868120 00 PTH=0.320876600 04 AZ=0.112201650 03

SMA=0.535000000 05 FCC=0.869158880 00 IMC=0.300000000 02 LAM=0.450000000 02 APF=0.450000000 02 NCA=0.699490900 04

C3=0.607045790 01 TMET=0.180000000 03 APRG=0.100000000 06 PAN=0.100000000 03 PERH=0.378983600 02 TPERH=0.789464000 00

VENUS CENTERED CENTRAL BODY MEAN EARTH ECLIPTIC AND EQUINOX OF 1950

X=0.669871810 06 Y=0.933012690 05 Z=0.35353440 05 NX=0.608201270 00 NY=0.436673150 01 NZ=0.230370000 00

R=0.100000000 06 DEC=0.207048160 02 RA=0.941069980 02 V=0.651868120 00 PTH=0.320876600 04 AZ=0.112201650 03

SMA=0.535000000 05 FCC=0.869158880 00 IMC=0.300000000 02 LAM=0.450000000 02 APF=0.450000000 02 NCA=0.699490900 04

C3=0.607045790 01 TMET=0.180000000 03 APRG=0.100000000 06 PAN=0.100000000 03 PERH=0.378983600 02 TPERH=0.789464000 00

VENUS CENTERED TRUE ECLIPTIC AND EQUINOX OF DATE

X=0.617861770 04 Y=0.998990030 05 Z=0.468162030 04 NX=0.608463450 00 NY=0.484523430 01 NZ=0.228815760 00

R=0.100000000 06 DEC=0.268335170 01 RA=0.935662730 02 V=0.651868120 00 PTH=0.320911650 04 AZ=0.110573010 03

SMA=0.535000000 05 FCC=0.869158880 00 IMC=0.300000000 02 LAM=0.450000000 02 APF=0.450000000 02 NCA=0.699490900 04

C3=0.607045790 01 TMET=0.180000000 03 APRG=0.100000000 06 PAN=0.100000000 03 PERH=0.378983600 02 TPERH=0.789464000 00

SUN CENTERED TRUE ECLIPTIC AND EQUINOX OF DATE

X=0.450202240 08 Y=0.988206570 08 Z=0.122527270 07 NX=0.322322050 02 NY=0.167301730 02 NZ=0.227658860 01

R=0.108599470 09 DEC=0.644452960 00 RA=0.114492830 03 V=0.359103560 02 PTH=0.266367660 01 AZ=0.936430000 02

NUMBER OF STEPS IS 0.100000000 01

MARCH 14, 1971, 13HRS, 54MIN, 18.225FC

JULIAN DATE 2441023.07437524

VENUS CENTERED CENTRAL BODY MEAN EARTH ECLIPTIC AND EQUINOX OF 1950

X=0.669871810 06 Y=0.933012690 05 Z=0.35353440 05 NX=0.608201270 00 NY=0.436673150 01 NZ=0.230370000 00

R=0.100000000 06 DEC=0.207048160 02 RA=0.941069980 02 V=0.651868120 00 PTH=0.320876600 04 AZ=0.112201650 03

SMA=0.535000000 05 FCC=0.869158880 00 IMC=0.300000000 02 LAM=0.450000000 02 APF=0.450000000 02 NCA=0.699490900 04

C3=0.607045790 01 TMET=0.180000000 03 APRG=0.100000000 06 PAN=0.100000000 03 PERH=0.378983600 02 TPERH=0.789464000 00

VENUS CENTERED TRUE ECLIPTIC AND EQUINOX OF DATE

X=0.617861770 04 Y=0.997189570 05 Z=0.468162030 04 NX=0.607660250 00 NY=0.480396460 01 NZ=0.228815760 00

R=0.100000000 06 DEC=0.267154710 01 RA=0.935162410 02 V=0.651868120 00 PTH=0.320876600 04 AZ=0.110573010 03

SMA=0.535000000 05 FCC=0.869158880 00 IMC=0.300000000 02 LAM=0.450000000 02 APF=0.450000000 02 NCA=0.699490900 04

C3=0.607045790 01 TMET=0.180000000 03 APRG=0.100000000 06 PAN=0.100000000 03 PERH=0.378983600 02 TPERH=0.789464000 00

SUN CENTERED TRUE ECLIPTIC AND EQUINOX OF DATE

X=0.406627210 08 Y=0.100728030 08 Z=0.967655110 06 NX=0.328784820 02 NY=0.133171350 02 NZ=0.227149380 01

R=0.108630070 09 DEC=0.499731520 00 RA=0.111983350 03 V=0.359087860 02 PTH=0.587391660 01 AZ=0.936641740 02

NUMBER OF STEPS IS 0.383000000 03

MARCH 16, 1971, 3HRS, 44MIN, 30.3735FC

JULIAN DATE 2441026.69877747

VENUS CENTERED CENTRAL BODY MEAN EARTH ECLIPTIC AND EQUINOX OF 1950

X=0.669871810 06 Y=0.933012690 05 Z=0.35353440 05 NX=0.608201270 00 NY=0.436673150 01 NZ=0.230370000 00

R=0.100000000 06 DEC=0.207048160 02 RA=0.941069980 02 V=0.651868120 00 PTH=0.320876600 04 AZ=0.112201650 03

SMA=0.535000000 05 FCC=0.869158880 00 IMC=0.300000000 02 LAM=0.450000000 02 APF=0.450000000 02 NCA=0.699490900 04

C3=0.607045790 01 TMET=0.180000000 03 APRG=0.100000000 06 PAN=0.100000000 03 PERH=0.378983600 02 TPERH=0.789464000 00

VENUS CENTERED TRUE ECLIPTIC AND EQUINOX OF DATE

X=0.607363500 04 Y=0.997371500 05 Z=0.468162030 04 NX=0.608463450 00 NY=0.484523430 01 NZ=0.228815760 00

R=0.100000000 06 DEC=0.265928000 01 RA=0.935662730 02 V=0.651868120 00 PTH=0.320911650 04 AZ=0.110573010 03

SMA=0.535000000 05 FCC=0.869158880 00 IMC=0.300000000 02 LAM=0.450000000 02 APF=0.450000000 02 NCA=0.699490900 04

C3=0.607045790 01 TMET=0.180000000 03 APRG=0.100000000 06 PAN=0.100000000 03 PERH=0.378983600 02 TPERH=0.789464000 00

SUN CENTERED TRUE ECLIPTIC AND EQUINOX OF DATE

X=0.422265360 08 Y=0.107464000 08 Z=0.967655110 06 NX=0.333821160 02 NY=0.118796420 02 NZ=0.227149380 01

R=0.108630070 09 DEC=0.352134000 00 RA=0.109675790 03 V=0.355063860 02 PTH=0.907168500 01 AZ=0.936641740 02

NUMBER OF STEPS IS 0.301000000 03

MARCH 16, 1971, 23HRS, 59MIN, 59.9905FC

JULIAN DATE 2441027.69999900

VENUS CENTERED CENTRAL BODY MEAN EARTH ECLIPTIC AND EQUINOX OF 1950

X=0.669871810 06 Y=0.933012690 05 Z=0.35353440 05 NX=0.608201270 00 NY=0.436673150 01 NZ=0.230370000 00

R=0.100000000 06 DEC=0.207048160 02 RA=0.941069980 02 V=0.651868120 00 PTH=0.320876600 04 AZ=0.112201650 03

SMA=0.535000000 05 FCC=0.869158880 00 IMC=0.300000000 02 LAM=0.450000000 02 APF=0.450000000 02 NCA=0.699490900 04

C3=0.607045790 01 TMET=0.180000000 03 APRG=0.100000000 06 PAN=0.100000000 03 PERH=0.378983600 02 TPERH=0.789464000 00

VENUS CENTERED TRUE ECLIPTIC AND EQUINOX OF DATE

X=0.607363500 04 Y=0.997371500 05 Z=0.468162030 04 NX=0.608463450 00 NY=0.484523430 01 NZ=0.228815760 00

R=0.100000000 06 DEC=0.265928000 01 RA=0.935662730 02 V=0.651868120 00 PTH=0.320911650 04 AZ=0.110573010 03

SMA=0.535000000 05 FCC=0.869158880 00 IMC=0.300000000 02 LAM=0.450000000 02 APF=0.450000000 02 NCA=0.699490900 04

C3=0.607045790 01 TMET=0.180000000 03 APRG=0.100000000 06 PAN=0.100000000 03 PERH=0.378983600 02 TPERH=0.789464000 00

SUN CENTERED TRUE ECLIPTIC AND EQUINOX OF DATE

X=0.422265360 08 Y=0.107464000 08 Z=0.967655110 06 NX=0.333821160 02 NY=0.118796420 02 NZ=0.227149380 01

R=0.108630070 09 DEC=0.352134000 00 RA=0.109675790 03 V=0.355063860 02 PTH=0.907168500 01 AZ=0.936641740 02

NUMBER OF STEPS IS 0.301000000 03

MARCH 16, 1971, 23HRS, 59MIN, 59.9905FC

JULIAN DATE 2441027.69999900

VENUS CENTERED CENTRAL BODY MEAN EARTH ECLIPTIC AND EQUINOX OF 1950

X=0.669871810 06 Y=0.933012690 05 Z=0.35353440 05 NX=0.608201270 00 NY=0.436673150 01 NZ=0.230370000 00

R=0.100000000 06 DEC=0.207048160 02 RA=0.941069980 02 V=0.651868120 00 PTH=0.320876600 04 AZ=0.112201650 03

SMA=0.535000000 05 FCC=0.869158880 00 IMC=0.300000000 02 LAM=0.450000000 02 APF=0.450000000 02 NCA=0.699490900 04

C3=0.607045790 01 TMET=0.180000000 03 APRG=0.100000000 06 PAN=0.100000000 03 PERH=0.378983600 02 TPERH=0.789464000 00

VENUS CENTERED TRUE ECLIPTIC AND EQUINOX OF DATE

X=0.607363500 04 Y=0.997371500 05 Z=0.468162030 04 NX=0.608463450 00 NY=0.484523430 01 NZ=0.228815760 00

R=0.100000000 06 DEC=0.265928000 01 RA=0.935662730 02 V=0.651868120 00 PTH=0.320911650 04 AZ=0.110573010 03

SMA=0.535000000 05 FCC=0.869158880 00 IMC=0.300000000 02 LAM=0.450000000 02 APF=0.450000000 02 NCA=0.699490900 04

C3=0.607045790 01 TMET=0.180000000 03 APRG=0.100000000 06 PAN=0.100000000 03 PERH=0.378983600 02 TPERH=0.789464000 00

SUN CENTERED TRUE ECLIPTIC AND EQUINOX OF DATE

X=0.422265360 08 Y=0.107464000 08 Z=0.967655110 06 NX=0.333821160 02 NY=0.118796420 02 NZ=0.227149380 01

R=0.108630070 09 DEC=0.352134000 00 RA=0.109675790 03 V=0.355063860 02 PTH=0.907168500 01 AZ=0.936641740 02

NUMBER OF STEPS IS 0.301000000 03

CASE 2 Periapsis Printout*

The only difference here from case 1 is the input array c(776), which now requests output at periapsis. Notice that the initial position was at periapsis.

*Periapsis printout is a form of exact print and requires restarting the integrator.

750	U.5350000000 05	751	U.6661500000 00	752	U.0	753	U.6500000000 02
754	U.3000000000 02	755	U.4500000000 02	756	U.7103130000 04	757	U.0
759	U.7103170000 04	760	U.0	761	U.6000000000 01	763	U.1000000000 04
764	U.0	766	U.4000000000 01	775	U.1000000000 01	776	U.1000000000 01
777	U.1001010000 00	0	U.0	0	U.0	0	U.0

SHANNON IS NOT REQUESTED

HARMONICS OF EARTH IS INCLUDED

HARMONICS OF MOON IS INCLUDED

HARMONICS OF MARS IS INCLUDED

SOLAR RADIATION PRESSURE IS NOT INCLUDED

INPUT IN MEAN FOR AMN FOR 1950

MARCH 13, 1971, 13HRS, 05MIN, U. USFC

X U.4409100000 03	Y U.6551000000 04	Z U.2476073000 06	DX U.8000000000 01	DY U.6230130000 01	DZ U.3292643100 01
R U.6999999900 06	DEC U.2070401200 02	HA U.8509330000 02	V U.9317401000 01	PTM U.8000000000 01	AZ U.6779230000 02

JULIAN DATE 2441023.50000000

PTM U.8000000000 01

MARCH 13, 1971, 13HRS, 05MIN, U. USFC

JULIAN DATE 2441023.50000000

VENUS CENTERED CENTRAL BODY MEAN EARTH EPOCH AND EQUINOX OF 1950

X U.4409100000 03	Y U.6551000000 04	Z U.2476073000 06	DX U.8000000000 01	DY U.6230130000 01	DZ U.3292643100 01
R U.6999999900 06	DEC U.2070401200 02	HA U.8509330000 02	V U.9317401000 01	PTM U.8000000000 01	AZ U.6779230000 02
SMA U.5350000000 05	FCC U.8000000000 00	INC U.3000000000 02	LAM U.4500000000 02	APF U.6500000000 02	RCA U.6000000000 06
C3-U.6070505000 01	THET U.0	APRG U.1000000000 06	MAN U.5951104000 16	PERM U.3700000000 02	TPER U.0

VENUS CENTERED TIME ECLIPIC AND EQUINOX OF DATE

X U.4325030000 03	Y U.6097000000 04	Z U.2277130000 06	DX U.8000000000 01	DY U.6021070000 01	DZ U.3200000000 01
R U.6999999900 06	DEC U.2060000000 02	HA U.8000000000 02	V U.9317401000 01	PTM U.8000000000 01	AZ U.6779230000 02
SMA U.5350000000 05	FCC U.8000000000 00	INC U.3000000000 02	LAM U.4500000000 02	APF U.6500000000 02	RCA U.6000000000 06
C3-U.6070505000 01	THET U.0	APRG U.1000000000 06	MAN U.5951104000 16	PERM U.3700000000 02	TPER U.0

SUN CENTERED TIME ECLIPIC AND EQUINOX OF DATE

X U.4501301000 03	Y U.0000000000 04	Z U.1220200000 06	DX U.2200000000 01	DY U.1000000000 01	DZ U.1200000000 01
R U.1000000000 06	DEC U.0000000000 02	HA U.1000000000 02	V U.2000000000 01	PTM U.1000000000 01	AZ U.0000000000 02

NUMBER OF STEPS IS 0.1000000000 01

JULIAN DATE 2441023.50000000

MARCH 14, 1971, 13HRS, 05MIN, 15.3945SEC

VENUS CENTERED CENTRAL BODY MEAN EARTH EPOCH AND EQUINOX OF 1950

X U.4409100000 03	Y U.6551000000 04	Z U.2476073000 06	DX U.8000000000 01	DY U.6230130000 01	DZ U.3292643100 01
R U.6999999900 06	DEC U.2070401200 02	HA U.8509330000 02	V U.9317401000 01	PTM U.8000000000 01	AZ U.6779230000 02
SMA U.5350000000 05	FCC U.8000000000 00	INC U.3000000000 02	LAM U.4500000000 02	APF U.6500000000 02	RCA U.6000000000 06
C3-U.6070505000 01	THET U.0	APRG U.1000000000 06	MAN U.5951104000 16	PERM U.3700000000 02	TPER U.0

VENUS CENTERED TIME ECLIPIC AND EQUINOX OF DATE

X U.4270000000 03	Y U.6097000000 04	Z U.2277130000 06	DX U.8000000000 01	DY U.6021070000 01	DZ U.3200000000 01
R U.6999999900 06	DEC U.2060000000 02	HA U.8000000000 02	V U.9317401000 01	PTM U.8000000000 01	AZ U.6779230000 02
SMA U.5350000000 05	FCC U.8000000000 00	INC U.3000000000 02	LAM U.4500000000 02	APF U.6500000000 02	RCA U.6000000000 06
C3-U.6070505000 01	THET U.0	APRG U.1000000000 06	MAN U.5951104000 16	PERM U.3700000000 02	TPER U.0

SUN CENTERED TIME ECLIPIC AND EQUINOX OF DATE

X U.4000000000 03	Y U.0000000000 04	Z U.1220200000 06	DX U.2200000000 01	DY U.1000000000 01	DZ U.1200000000 01
R U.1000000000 06	DEC U.0000000000 02	HA U.1000000000 02	V U.2000000000 01	PTM U.1000000000 01	AZ U.0000000000 02

NUMBER OF STEPS IS 0.2100000000 03

JULIAN DATE 2441026.06010457

MARCH 16, 1971, 23HRS, 50MIN, 33.305SEC

VENUS CENTERED CENTRAL BODY MEAN EARTH EPOCH AND EQUINOX OF 1950

X U.4501301000 03	Y U.0000000000 04	Z U.1220200000 06	DX U.2200000000 01	DY U.1000000000 01	DZ U.1200000000 01
R U.1000000000 06	DEC U.0000000000 02	HA U.1000000000 02	V U.2000000000 01	PTM U.1000000000 01	AZ U.0000000000 02
SMA U.5350000000 05	FCC U.8000000000 00	INC U.3000000000 02	LAM U.4500000000 02	APF U.6500000000 02	RCA U.6000000000 06
C3-U.6070505000 01	THET U.0	APRG U.1000000000 06	MAN U.5951104000 16	PERM U.3700000000 02	TPER U.0

VENUS CENTERED TIME ECLIPIC AND EQUINOX OF DATE

X U.4270000000 03	Y U.6097000000 04	Z U.2277130000 06	DX U.8000000000 01	DY U.6021070000 01	DZ U.3200000000 01
R U.6999999900 06	DEC U.2060000000 02	HA U.8000000000 02	V U.9317401000 01	PTM U.8000000000 01	AZ U.6779230000 02
SMA U.5350000000 05	FCC U.8000000000 00	INC U.3000000000 02	LAM U.4500000000 02	APF U.6500000000 02	RCA U.6000000000 06
C3-U.6070505000 01	THET U.0	APRG U.1000000000 06	MAN U.5951104000 16	PERM U.3700000000 02	TPER U.0

SUN CENTERED TIME ECLIPIC AND EQUINOX OF DATE

X U.4000000000 03	Y U.0000000000 04	Z U.1220200000 06	DX U.2200000000 01	DY U.1000000000 01	DZ U.1200000000 01
R U.1000000000 06	DEC U.0000000000 02	HA U.1000000000 02	V U.2000000000 01	PTM U.1000000000 01	AZ U.0000000000 02

NUMBER OF STEPS IS 0.2100000000 03

JULIAN DATE 2441027.50000000

MARCH 16, 1971, 23HRS, 50MIN, 59.999SEC

VENUS CENTERED CENTRAL BODY MEAN EARTH EPOCH AND EQUINOX OF 1950

X U.4501301000 03	Y U.0000000000 04	Z U.1220200000 06	DX U.2200000000 01	DY U.1000000000 01	DZ U.1200000000 01
R U.1000000000 06	DEC U.0000000000 02	HA U.1000000000 02	V U.2000000000 01	PTM U.1000000000 01	AZ U.0000000000 02
SMA U.5350000000 05	FCC U.8000000000 00	INC U.3000000000 02	LAM U.4500000000 02	APF U.6500000000 02	RCA U.6000000000 06
C3-U.6070505000 01	THET U.0	APRG U.1000000000 06	MAN U.5951104000 16	PERM U.3700000000 02	TPER U.0

VENUS CENTERED TIME ECLIPIC AND EQUINOX OF DATE

X U.4270000000 03	Y U.6097000000 04	Z U.2277130000 06	DX U.8000000000 01	DY U.6021070000 01	DZ U.3200000000 01
R U.6999999900 06	DEC U.2060000000 02	HA U.8000000000 02	V U.9317401000 01	PTM U.8000000000 01	AZ U.6779230000 02
SMA U.5350000000 05	FCC U.8000000000 00	INC U.3000000000 02	LAM U.4500000000 02	APF U.6500000000 02	RCA U.6000000000 06
C3-U.6070505000 01	THET U.0	APRG U.1000000000 06	MAN U.5951104000 16	PERM U.3700000000 02	TPER U.0

SUN CENTERED TIME ECLIPIC AND EQUINOX OF DATE

X U.4000000000 03	Y U.0000000000 04	Z U.1220200000 06	DX U.2200000000 01	DY U.1000000000 01	DZ U.1200000000 01
R U.1000000000 06	DEC U.0000000000 02	HA U.1000000000 02	V U.2000000000 01	PTM U.1000000000 01	AZ U.0000000000 02

NUMBER OF STEPS IS 0.2000000000 02

CASE 3 Printout at Exact Intervals[†]

This case represents printout requested at intervals of exactly 1-1/2 days. While this feature may be extremely useful in some cases, it is inefficient in that it requires the integrator to restart after every printout.

The differences in input are:

- (1) c(761) is 1.5 since printout is wanted at exactly 1.5 day intervals.
- (2) c(762) is 2., which is the total days (4) divided by Δt (1.5) and truncated. Note that $c(762) * \Delta t \neq 4$ and therefore TRIP gives a final printout after 4 days which is at the requested stop time.
- (3) c(776) uses the built-in value of 0. since printout is not wanted at perigee or apogee.

[†] Do not request exact printout and printout at apoapsis or periapsis in the same run. TRIP can not handle this multiple type output.

CASE 4 Printout At Approximate Intervals

This case requests printout at approximately 1.5 day intervals. This means that printout is obtained at the first step of the integrator beyond the time actually requested. This type of printout does not require the numerical integrator to restart and is therefore much more efficient than any of the types discussed in cases 1-3. Where possible it should be used instead of the exact printouts.

The differences in input are

- (1) c(761) is set equal to the total time of 4 days.
- (2) c(762) use the built-in value of 1. and therefore does not appear in the input.
- (3) c(763) uses the built-in value of 0. and therefore does not appear in the input.
- (4) c(764) is set to 1.5 days in seconds.

Note that the printout of the number of integration steps taken is cumulative and represents the number of total steps taken from epoch, whereas in the exact printouts of cases 1 through 3 it represents the steps taken from the last printout.

750	0.535000000	05	751	0.535000000	05	752	0.535000000	05	753	0.535000000	05
754	0.535000000	05	755	0.535000000	05	756	0.535000000	05	757	0.535000000	05
758	0.535000000	05	759	0.535000000	05	760	0.535000000	05	761	0.535000000	05
762	0.535000000	05	763	0.535000000	05	764	0.535000000	05	765	0.535000000	05

SHADOW IS NOT REQUESTED

HARMONICS OF EARTH IS INCLUDED

HARMONICS OF MARS IS INCLUDED

HARMONICS OF JUPITER IS INCLUDED

SOLAR RADIATION PRESSURE IS NOT INCLUDED

INPUT IN MEAN FO AND FO OF 1950

MARCH 13, 1971, 0HRS, 0MIN, 0. USFC	JULIAN DATE 2441023.50000000
X 0.468910820 03	Y 0.653100880 04
R 0.699999999 04	DEC 0.207048120 02

MARCH 13, 1971, 0HRS, 0MIN, 0. USFC

VENUS CENTERED CENTRAL BODY MEAN EARTH EQUATOR AND EQUINOX OF 1950	JULIAN DATE 2441023.50000000
X 0.468910820 03	Y 0.653100880 04
R 0.699999999 04	DEC 0.207048120 02
SMA 0.535000000 05	FCC 0.869158880 06
C3-0.607045790 01	THET 0.0

VENUS CENTERED TRUE ECLIPTIC AND EQUINOX OF DATE	JULIAN DATE 2441023.50000000
X 0.432503800 03	Y 0.697893570 04
R 0.699999999 04	DEC 0.268335340 01
SMA 0.535000000 05	FCC 0.869158880 06
C3-0.607045740 01	THET 0.0

SIN CENTERED TRUE ECLIPTIC AND EQUINOX OF DATE	JULIAN DATE 2441023.50000000
X 0.450136130 03	Y 0.697893570 04
R 0.699999999 04	DEC 0.268335340 01
C3-0.607045740 01	THET 0.0

NUMBER OF STEPS IS 0.100000000 01

MARCH 14, 1971, 12HRS, 2MIN, 39.4685FC

VENUS CENTERED CENTRAL BODY MEAN EARTH EQUATOR AND EQUINOX OF 1950	JULIAN DATE 2441025.00164570
X 0.202999962 05	Y 0.181429300 05
R 0.314328270 05	DEC 0.299841010 02
SMA 0.535000000 05	FCC 0.869158880 06
C3-0.607057210 01	THET 0.132250410 03

VENUS CENTERED TRUE ECLIPTIC AND EQUINOX OF DATE	JULIAN DATE 2441025.00164570
X 0.204191820 05	Y 0.227886680 05
R 0.314328270 05	DEC 0.132250410 02
SMA 0.535000000 05	FCC 0.869158880 06
C3-0.607057200 01	THET 0.132250410 03

SIN CENTERED TRUE ECLIPTIC AND EQUINOX OF DATE	JULIAN DATE 2441025.00164570
X 0.408519800 05	Y 0.100941940 05
R 0.108547220 05	DEC 0.501077740 00
C3-0.607057200 01	THET 0.132250410 03

NUMBER OF STEPS IS 0.162000000 03

MARCH 16, 1971, 0HRS, 2MIN, 25.9105FC

VENUS CENTERED CENTRAL BODY MEAN EARTH EQUATOR AND EQUINOX OF 1950	JULIAN DATE 2441026.50164570
X 0.217539570 05	Y 0.278615680 05
R 0.501021500 05	DEC 0.291587220 02
SMA 0.535000000 05	FCC 0.869158880 06
C3-0.607044530 01	THET 0.162286620 03

VENUS CENTERED TRUE ECLIPTIC AND EQUINOX OF DATE	JULIAN DATE 2441026.50164570
X 0.219861140 05	Y 0.444256450 05
R 0.501021500 05	DEC 0.132250410 02
SMA 0.535000000 05	FCC 0.869158880 06
C3-0.607044520 01	THET 0.162286620 03

SIN CENTERED TRUE ECLIPTIC AND EQUINOX OF DATE	JULIAN DATE 2441026.50164570
X 0.366429750 05	Y 0.102224100 05
R 0.108547220 05	DEC 0.501077740 00
C3-0.607044520 01	THET 0.162286620 03

NUMBER OF STEPS IS 0.345000000 03

MARCH 18, 1971, 23HRS, 59MIN, 59.9995FC

VENUS CENTERED CENTRAL BODY MEAN EARTH EQUATOR AND EQUINOX OF 1950	JULIAN DATE 2441027.50000000
X 0.394999999 05	Y 0.278615680 05
R 0.999999999 05	DEC 0.213874200 02
SMA 0.535000000 05	FCC 0.869158880 06
C3-0.607044530 01	THET 0.170996730 03

VENUS CENTERED TRUE ECLIPTIC AND EQUINOX OF DATE	JULIAN DATE 2441027.50000000
X 0.394999999 05	Y 0.278615680 05
R 0.999999999 05	DEC 0.213874200 02
SMA 0.535000000 05	FCC 0.869158880 06
C3-0.607044530 01	THET 0.170996730 03

SIN CENTERED TRUE ECLIPTIC AND EQUINOX OF DATE	JULIAN DATE 2441027.50000000
X 0.394999999 05	Y 0.278615680 05
R 0.999999999 05	DEC 0.213874200 02
C3-0.607044530 01	THET 0.170996730 03

NUMBER OF STEPS IS 0.535000000 03

CASE 5 First and Last Point Printout

This case represents the most efficient type of run but also the one that gives the least information, being useful only when the final point is all that is desired. Note that the total steps taken will be the same as for case 4. The differences in input from case 4 are:

- (1) c(763) is again set to 100 000.
- (2) c(764) is set to 0.

750	0.54500000 05	751	0.66015000 00	752	0.00	753	0.45000000 02
754	0.30000000 02	755	0.48000000 02	756	0.47131000 04	757	0.00
758	0.71031000 04	759	0.00	761	0.46000000 01	763	0.10000000 06
764	0.00	766	0.44000000 01	775	0.41000000 01	777	0.10010100 06

SHADOW IS NOT REQUESTED

HARMONICS OF EARTH IS INCLUDED

HARMONICS OF MOON IS INCLUDED

HARMONICS OF MARS IS INCLUDED

SOLAR RADIATION PRESSURE IS NOT INCLUDED

INPUT IN MEAN EO AND EO OF 1950

MARCH 13, 1971, 00HRS, 00MIN, 0.0 SEC	JULIAN DATE 2441023.50000000
X 0.468910820 03 Y 0.653108800 04 Z 0.247487300 06	DX=0.668854920 01 DY=0.623813050 00 DZ 0.329243130 01
R 0.669999990 04 DEC 0.207048120 02	PTH 0.406047430 06 AZ 0.677923450 02

MARCH 13, 1971, 00HRS, 00MIN, 0.0 SEC

JULIAN DATE 2441023.50000000

VENUS CENTERED CENTRAL BODY MEAN EARTH ECLIPTIC AND EQUINOX OF DATE

X 0.468910820 03 Y 0.653108800 04 Z 0.247487300 06	DX=0.668854920 01	DY=0.623813050 00	DZ 0.329243130 01
R 0.669999990 04 DEC 0.207048120 02	VA 0.654933970 02	PTH 0.406047430 06	AZ 0.677923450 02
SMA 0.535000000 05 FCC 0.669158800 00	INC 0.300000000 02	LAN 0.440000000 02	APF 0.450000000 02

VENUS CENTERED TRUE ECLIPTIC AND EQUINOX OF DATE

X 0.432503800 03 Y 0.697893570 04 Z 0.247713400 06	DX=0.669233480 01	DY 0.602382660 00	DZ 0.326870630 01
R 0.669999990 04 DEC 0.207048120 02	VA 0.654933970 02	PTH 0.406047430 06	AZ 0.694268800 02
SMA 0.535000000 05 FCC 0.669158800 00	INC 0.300000000 02	LAN 0.440000000 02	APF 0.450000000 02

SUN CENTERED TRUE ECLIPTIC AND EQUINOX OF DATE

X 0.450136130 03 Y 0.987134790 04 Z 0.122026340 07	DX 0.229314070 02	DY=0.139895300 02	DZ 0.124102380 01
R 0.108499600 09 DEC 0.644402490 00	VA=0.116513000 03	PTH 0.680060300 01	AZ 0.676133550 02

NUMBER OF STEPS IS 0.10000000 01

MARCH 16, 1971, 23HRS, 59MIN, 59.9999 SEC

JULIAN DATE 2441021.50000000

VENUS CENTERED CENTRAL BODY MEAN EARTH ECLIPTIC AND EQUINOX OF DATE

X 0.394994880 04 Y 0.928746420 05 Z 0.262154760 05	DX 0.613666240 01	DY 0.617487580 00	DZ 0.180111660 00
R 0.998003750 05 DEC 0.213387420 02	VA=0.640050000 00	PTH=0.105579600 02	AZ 0.110887660 03
SMA 0.535151420 05 FCC 0.669775940 00	INC 0.300555140 02	LAN 0.440000000 02	APF 0.440000000 02

VENUS CENTERED TRUE ECLIPTIC AND EQUINOX OF DATE

X 0.342983760 04 Y 0.996793070 05 Z 0.263102570 06	DX 0.613223660 00	DY 0.610879730 01	DZ 0.254812530 00
R 0.998003750 05 DEC 0.208504600 01	VA=0.619070760 02	PTH=0.105579600 02	AZ 0.110713120 03
SMA 0.535151420 05 FCC 0.669775940 00	INC 0.298137050 02	LAN 0.439511950 02	APF 0.345519600 03

SUN CENTERED TRUE ECLIPTIC AND EQUINOX OF DATE

X 0.338319940 08 Y 0.103272780 09 Z 0.517308670 06	DX 0.436523800 02	DY=0.109644220 02	DZ 0.229372200 01
R 0.108676640 09 DEC 0.272738550 00	VA=0.109138710 03	PTH=0.100276860 00	AZ 0.938766000 02

NUMBER OF STEPS IS 0.53500000 03

CASE 6 Shadow Printout

This case is for an Earth satellite and includes printout of latitude and longitude of the satellite as well as shadow times. Note that, as explained earlier in the section on known bugs, the satellite was in shadow at the start and therefore the first shadow times are incorrect. This is obvious since the times show the spacecraft entering umbra first! The second sequence of shadow times is correct. Note also, that the oblateness effects of the Earth were included here. The input data differences from the previous cases are:

- (1) c(750) through c(755) are now state vector components.
- (2) c(758) shows that the state vector is referenced to the true Earth equator and equinox of date.
- (3) c(761), c(762) (built-in value), c(763), c(764) indicate that only the first and last points are requested.
- (4) c(765) indicates that shadow times are requested from the outset
- (5) c(766) is the built-in value indicating the Earth is the central body
- (6) c(775) is the built-in value indicating input is cartesian state vector.
- (7) c(777) is the built-in values for output options.

750 -0.60233880 04	751 0.66356000 03	752 -0.26647660 04	0 0.0
753 -0.19974716 01	754 -0.19244100 02	755 0.27291272 01	0 0.0
756 0.71031000 04	757 0.17060000 04	758 0.50000000 01	0 0.0
759 0.71031000 04	760 0.17060000 04	761 0.40000000 01	763 0.10000000 04
762 0.0	765 0.0	0 0.0	0 0.0

SHADOW IS REQUESTED

PARABOLICS OF EARTH IS INCLUDED

PARABOLICS OF MOON IS INCLUDED

PARABOLICS OF MARS IS INCLUDED

SOLAR RADIATION PRESSURE IS NOT INCLUDED

INPUT IN MEAN EQ AND EQ OF 1950

MARCH 10, 1971, 17HRS, 5MIN, 59.9995SEC

JULIAN DATE 2441021.21250000

X=0.60267703 04	Y=0.47207734 03	Z=0.26722306 04	DX=0.20406749 01	DY=0.10238251 02	DZ=0.27937168 01
R=0.66095109 04	BEC=0.23847320 02	BA=0.17552116 03	V=0.10806989 02	PTH=0.71412335 04	AZ=0.73582150 02

MARCH 10, 1971, 17HRS, 5MIN, 59.9995SEC

JULIAN DATE 2441021.21250000

EARTH CENTERED TIME EARTH EPOCH AND EPOCH OF DATE

X=0.60233880 04	Y=0.66356000 03	Z=0.26647660 04	DX=0.19974716 01	DY=0.10240190 02	DZ=0.27891272 01
R=0.66095109 04	BEC=0.23847320 02	BA=0.17579034 03	V=0.10806989 02	PTH=0.71412335 04	AZ=0.73582150 02
SMA=0.10623669 04	EC=0.93659132 00	INC=0.28477691 02	LAM=0.22985441 03	APF=0.30243082 03	RCA=0.66095109 04
CS=0.38240197 01	THET=0.0	APRG=0.20186787 04	MAN=0.36000000 03	PERH=0.03033203 02	TPRH=0.0

EARTH CENTERED CENTRAL BODY MEAN EARTH EPOCH AND EPOCH OF 1950

X=0.60267703 04	Y=0.47207734 03	Z=0.26722306 04	DX=0.20406749 01	DY=0.10238251 02	DZ=0.27937168 01
R=0.66095109 04	BEC=0.23847320 02	BA=0.17552116 03	V=0.10806989 02	PTH=0.71412335 04	AZ=0.73582150 02
SMA=0.10623669 04	EC=0.93659132 00	INC=0.28477691 02	LAM=0.22985441 03	APF=0.30243082 03	RCA=0.66095109 04
CS=0.38240197 01	THET=0.16617560 04	APRG=0.20186787 04	MAN=0.36000000 03	PERH=0.03033203 02	TPRH=0.22988780 04

EARTH FIXED LATITUDE(DEC)=0.23966010 02 LONGITUDE(DEC)=0.11157053 03

NUMBER OF STEPS IS 0.10000000 01

PROBE ENTERED EARTH PENUMBRA. TIME AND UNIT ARE GIVEN BELOW

MARCH 10, 1971, 17HRS, 16MIN, 23.1345SEC

JULIAN DATE 2441021.21971221

PROBE ENTERED EARTH UMRA. TIME AND UNIT ARE GIVEN BELOW

MARCH 10, 1971, 17HRS, 16MIN, 17.2225SEC

JULIAN DATE 2441021.21964278

PROBE HAS LEFT EARTH PENUMBRA. TIME AND UNIT ARE GIVEN BELOW

MARCH 10, 1971, 17HRS, 16MIN, 23.2145SEC

JULIAN DATE 2441021.21971313

PROBE HAS LEFT EARTH UMRA. TIME AND UNIT ARE GIVEN BELOW

MARCH 10, 1971, 17HRS, 16MIN, 17.3015SEC

JULIAN DATE 2441021.21964369

PROBE ENTERED EARTH PENUMBRA. TIME AND UNIT ARE GIVEN BELOW

MARCH 14, 1971, 13HRS, 5MIN, 59.9995SEC

JULIAN DATE 2441025.04789901

PROBE ENTERED EARTH UMRA. TIME AND UNIT ARE GIVEN BELOW

MARCH 14, 1971, 13HRS, 5MIN, 3.9055SEC

JULIAN DATE 2441025.04796187

PROBE HAS LEFT EARTH PENUMBRA. TIME AND UNIT ARE GIVEN BELOW

MARCH 14, 1971, 13HRS, 5MIN, 14.1755SEC

JULIAN DATE 2441025.04809062

PROBE HAS LEFT EARTH UMRA. TIME AND UNIT ARE GIVEN BELOW

MARCH 14, 1971, 13HRS, 5MIN, 20.2875SEC

JULIAN DATE 2441025.04804037

MARCH 14, 1971, 17HRS, 5MIN, 59.9995SEC

JULIAN DATE 2441025.21250000

EARTH CENTERED TIME EARTH EPOCH AND EPOCH OF DATE

X=0.38593026 05	Y=0.33610891 04	Z=0.26434414 04	DX=0.24901744 01	DY=0.73081724 00	DZ=0.13952991 01
R=0.58525363 05	BEC=0.29070716 02	BA=0.41088070 02	V=0.31251406 01	PTH=0.66095109 02	AZ=0.90108811 02
SMA=0.10529762 04	EC=0.93576683 00	INC=0.29070802 02	LAM=0.22448700 03	APF=0.30389537 03	RCA=0.66415671 04
CS=0.38550519 01	THET=0.16650836 03	APRG=0.20015340 04	MAN=0.14864521 02	PERH=0.01012125 02	TPRH=0.15817000 01

EARTH CENTERED CENTRAL BODY MEAN EARTH EPOCH AND EPOCH OF 1950

X=0.38650780 05	Y=0.33602054 04	Z=0.26435700 04	DX=0.24885445 01	DY=0.73067911 00	DZ=0.13897124 01
R=0.58525363 05	BEC=0.28482473 02	BA=0.41118879 02	V=0.31251406 01	PTH=0.66095109 02	AZ=0.90208820 02
SMA=0.10339767 04	EC=0.93576683 00	INC=0.28983106 02	LAM=0.22826797 03	APF=0.30389148 03	RCA=0.66415570 04
CS=0.38550519 01	THET=0.16650836 03	APRG=0.20015340 04	MAN=0.14864521 02	PERH=0.01012125 02	TPRH=0.15817000 01

EARTH FIXED LATITUDE(DEC)=0.29070716 02 LONGITUDE(DEC)=0.10925122 03

NUMBER OF STEPS IS 0.71100000 03

INCORRECT